

TABLE B1: Theoretical Calculation of East Quarry Leachate Concentration

Parameter	Waste Stream	Mass from Bulk Analysis (avg) (mg/kg)	Mass of Waste Stream in West Quarry (kg)	Total mass of parameter (mg)	% of mass of parameter (%)	Concentration in West Quarry Landfill Leachate During Recirculation		Recalculated Range in East Quarry leachate concentration			
						(min)	(max)	(min)	(max)		
Ammonia						(average)		(average)			
	AMW	38	1532881	58249478	3	23	-	213	3	-	31
	BOF	135	815766	110128410	7						
	CONS	69	1071819	73955511	4		162			23	
	Al Proc.	8270	173659	1436159930	86						
				1678493329							
Chloride											
	AMW	185	1532881	283582985	0	2210	-	10400	34	-	161
	BOF	188	815766	153364008	0						
	CONS	740	1071819	793146060	1		7508			116	
	Al Proc.	450000	173659	78146550000	98.5						
				79376643053							
TKN											
	AMW	540	1532881	827755740	22	102	-	221	51	-	110
	BOF	405	815766	330385230	9						
	CONS	650	1071819	696682350	19		174			87	
	Al Proc.	10800	173659	1875517200	50						
				3730340520							
Sodium											
	AMW	2510	1532881	3847531310	8	1320	-	6050	161	-	739
	BOF	1338	815766	1091494908	2						
	CONS	892	1071819	956062548	2		5154			629	
	Al Proc.	244000	173659	42372796000	88						
				48267884766							
Fluoride											
	AMW	14	1532881	21460334	33	1.2	-	2.7	0.6	-	1.5
	BOF	9	815766	7341894	11						
	CONS	5.5	1071819	5895004.5	9		1.85			1.0	
	Al Proc.	170	173659	29522030	46						
				64219262.5							
Aluminum											
	AMW	31266	1532881	47927057346	65	0	-	0.5	0.0	-	0.4
	BOF	1547	815766	1261990002	2						
	CONS	9398	1071819	10072954962	14		0.11			0.1	
	Al Proc.	83100	173659	14431062900	20						
				73693065210							
Copper											
	AMW	723	1532881	1108272963	63	0	-	0.01	0	-	0.01
	BOF	117	815766	95444622	5						
	CONS	101	1071819	108253719	6		0.0006			0.0004	
	Al Proc.	2620	173659	454986580	26						
				1766957884							
Chromium											
	AMW	78.00	1532881	119564718	50	0	-	0	0	-	0
	BOF	57	815766	46498662	19						
	CONS	44	1071819	47160036	20		0			0	
	Al Proc.	160	173659	27785440	12						
				241008856							
Titanium											
	AMW	590	1532881	904399790	70	0	-	0.013	0.00	-	0.012
	BOF	28	815766	22841448	2						
	CONS	202	1071819	216507438	17		0.002			0.002	
	Al Proc.	801	173659	139100859	11						
				1282849535							

AMW – approved mixed waste
BOF – basic oxygen furnace oxides

CONS – contaminated soils
Al. proc. – aluminum processing waste

Output from PHREEQE modelling of predicted East Quarry
Landfill Leachate

ELEMENTS
SPECIES
LOOK MIN

Taro - predicted leachate

0030011000 1 1 .00000

SOLUTION 1

33-II - Recirculation leachate minum aluminum processing waste effects

34 10 2 11.3 -1.00 10.0 1.00
 4 0.000D+00 5 0.000D+00 6 0.000D+00 7 0.000D+00 8 1.250D+00
 9 8.300D+00 10 3.897D+03 11 1.550D+03 12 0.000D+00 13 8.000D+03
 14 0.000D+00 15 0.000D+00 16 1.500D+00 17 0.000D+00 18 0.000D+00
 19 5.300D+02 20 0.000D+00 21 0.000D+00 22 0.000D+00 23 8.683D+02
 24 3.960D+03 25 0.000D+00 26 0.000D+00 27 0.000D+00 28 0.000D+00
 29 1.200D+02 30 6.101D+01 31 5.220D+00 32 0.000D+00 33 0.000D+00
 34 0.000D+00 35 0.000D+00 36 0.000D+00 37 0.000D+00

REACTION

23 -1.000 4.000

STEPS

.900E-02

SOLUTION NUMBER 1

33-II

TOTAL MOLALITIES OF ELEMENTS

ELEMENT	MOLALITY	LOG MOLALITY
BA	9.277802D-06	-5.0326
BR	1.058868D-04	-3.9752
TOT ALK	6.619775D-02	-1.1792
CA	3.942177D-02	-1.4043
CL	2.300219D-01	-.6382
F	8.048341D-05	-4.0943
K	1.381685D-02	-1.8596
N	1.427499D-02	-1.8454
NA	1.755869D-01	-.7555
S	1.273396D-03	-2.8950
SI	6.470528D-04	-3.1891
SR	6.072945D-05	-4.2166

----DESCRIPTION OF SOLUTION----

PH = 11.3000
 PE = -1.0000
 ACTIVITY H2O = .9917
 IONIC STRENGTH = .2782
 TEMPERATURE = 10.0000
 ELECTRICAL BALANCE = -1.6415D-02
 THOR = -9.9046D+00
 TOTAL ALKALINITY = 6.6198D-02
 ITERATIONS = 9
 TOTAL CARBON = 3.2655D-02

 DISTRIBUTION OF SPECIES

I	SPECIES	Z	MOLALITY	LOG MOLALITY	ACTIVITY	LOG ACTIVITY	GAMMA	LOG GAMMA
1	H+	1.0	6.77043D-12	-11.1694	5.01187D-12	-11.3000	7.40259D-01	-.1306
2	E-	-1.0	1.00000D+01	1.0000	1.00000D+01	1.0000	1.00000D+00	.0000
3	H2O	.0	9.91749D-01	-.0036	9.91749D-01	-.0036	1.00000D+00	.0000
8	BA 2+	2.0	9.26934D-06	-5.0330	2.78346D-06	-5.5554	3.00286D-01	-.5225
9	BR-	-1.0	1.05887D-04	-3.9752	7.83837D-05	-4.1058	7.40259D-01	-.1306
10	CO3 2-	-2.0	9.11420D-03	-2.0403	2.73687D-03	-2.5627	3.00286D-01	-.5225
11	CA 2+	2.0	2.00041D-02	-1.6989	6.74991D-03	-2.1707	3.37427D-01	-.4718
13	CL-	-1.0	2.30022D-01	-.6382	1.55753D-01	-.8076	6.77123D-01	-.1693
16	F-	-1.0	7.62140D-05	-4.1180	5.64181D-05	-4.2486	7.40259D-01	-.1306
19	K+	1.0	1.38036D-02	-1.8600	9.34672D-03	-2.0293	6.77123D-01	-.1693
23	NO3 -	-1.0	6.34656D-24	-23.1975	4.69810D-24	-23.3281	7.40259D-01	-.1306
24	NA+	1.0	1.71531D-01	-.7657	1.25715D-01	-.9006	7.32902D-01	-.1350
29	SO4 2-	-2.0	8.49319D-04	-3.0709	1.97092D-04	-3.7053	2.32059D-01	-.6344
30	H4SiO4	.0	3.61338D-05	-4.4421	3.85242D-05	-4.4143	1.06615D+00	.0278
31	SR 2+	2.0	6.06410D-05	-4.2172	1.82097D-05	-4.7397	3.00286D-01	-.5225
55	NH4 +	1.0	1.42388D-02	-1.8465	1.05404D-02	-1.9771	7.40259D-01	-.1306
56	NO2 -	-1.0	2.98736D-14	-13.5247	2.21142D-14	-13.6553	7.40259D-01	-.1306
58	SO3 2-	-2.0	4.82320D-28	-27.3167	1.44834D-28	-27.8391	3.00286D-01	-.5225
65	OH-	-1.0	8.14416D-04	-3.0892	6.02879D-04	-3.2198	7.40259D-01	-.1306
66	H3SiO4 -	-1.0	5.34115D-04	-3.2724	3.95384D-04	-3.4030	7.40259D-01	-.1306
67	H2SiO4--	-2.0	7.68038D-05	-4.1146	2.30631D-05	-4.6371	3.00286D-01	-.5225
75	NH4SO4 -	-1.0	3.61523D-05	-4.4419	2.67621D-05	-4.5725	7.40259D-01	-.1306
84	CAOH +	1.0	1.24148D-04	-3.9061	9.19014D-05	-4.0367	7.40259D-01	-.1306
85	CAHCO3 +	1.0	2.52100D-05	-4.5984	1.86619D-05	-4.7290	7.40259D-01	-.1306
86	CACO3 AQ	.0	1.90423D-02	-1.7203	2.03020D-02	-1.6925	1.06615D+00	.0278
87	CASO4 AQ	.0	2.22879D-04	-3.6519	2.37623D-04	-3.6241	1.06615D+00	.0278
91	CAF +	1.0	3.19051D-06	-5.4961	2.36181D-06	-5.6268	7.40259D-01	-.1306
92	NACO3 -	-1.0	3.88378D-03	-2.4107	2.87500D-03	-2.5414	7.40259D-01	-.1306
93	NAHCO3 A	.0	1.94457D-05	-4.7112	2.07320D-05	-4.6834	1.06615D+00	.0278
94	NASO4 -	-1.0	1.51770D-04	-3.8188	1.12349D-04	-3.9494	7.40259D-01	-.1306
96	NAF AQ	.0	1.07892D-06	-5.9670	1.15029D-06	-5.9392	1.06615D+00	.0278
97	KS04 -	-1.0	1.32763D-05	-4.8769	9.82791D-06	-5.0075	7.40259D-01	-.1306
134	SROH +	1.0	8.84088D-08	-7.0535	6.54454D-08	-7.1841	7.40259D-01	-.1306
135	BAOH +	1.0	8.46215D-09	-8.0725	6.26419D-09	-8.2031	7.40259D-01	-.1306
272	HCO3 -	-1.0	5.70487D-04	-3.2438	4.22308D-04	-3.3744	7.40259D-01	-.1306
273	H2CO3 AQ	.0	5.75806D-09	-8.2397	6.13898D-09	-8.2119	1.06615D+00	.0278
274	HSO4 -	-1.0	8.63444D-14	-13.0638	6.39172D-14	-13.1944	7.40259D-01	-.1306
275	HF AQ	.0	2.87244D-13	-12.5417	3.06246D-13	-12.5139	1.06615D+00	.0278
276	HF2 -	-1.0	8.04974D-17	-16.0942	5.95889D-17	-16.2248	7.40259D-01	-.1306
277	H2F2 AQ	.0	4.39559D-25	-24.3570	4.68638D-25	-24.3292	1.06615D+00	.0278

---- LOOK MIN IAP ----

PHASE	LOG IAP	LOG KT	LOG IAP/KT
ANHYDRIT	-5.8760	-4.4936	-1.3824
ARAGONIT	-4.7334	-8.2107	3.4773
BAF2	-14.0526	-5.7988	-8.2537
BARITE	-9.2607	-10.2238	.9631
CALCITE	-4.7334	-8.4064	3.6730
CELESTIT	-8.4450	-6.4518	-1.9933
CHALCEDO	-4.4071	-3.6990	-.7081
CRISTOBA	-4.4071	-3.8036	-.6035
FLUORITE	-10.6679	-11.1429	.4750
GYPSUM	-5.8832	-4.8601	-1.0231
HALITE	-1.7082	1.5443	-3.2525
MAGADIIT	-20.4681	-14.3000	-6.1681
MIRABILI	-5.5425	-1.8474	-3.6952
NATRON	-4.4000	-1.9212	-2.4788
QUARTZ	-4.4071	-4.2515	-.1556
SiO2(A,G	-4.4071	-2.8523	-1.5548
SiO2(A,P	-4.4071	-2.8523	-1.5548
SRF2	-13.2369	-8.5885	-4.6483
STRONTIA	-7.3024	-9.2232	1.9208
THENARDI	-5.5066	-.1579	-5.3487
THERMONA	-4.3676	.2387	-4.6063
WITHERIT	-8.1182	-8.6040	.4858
SULFUR	-88.0909	-37.9421	-50.1488
LIME	20.4257	34.5962	-14.1705
PORTLAND	20.4221	23.8617	-3.4396
WOLLASTO	16.0186	13.7572	2.2615
P-WOLLST	16.0186	14.6681	1.3505
CA-OLIVI	36.4443	39.7736	-3.3292
LARNITE	36.4443	41.3626	-4.9182
CA3SiO5	56.8700	77.9987	-21.1287
NA2SO3	-26.1030	5.0649	-31.1679
K2SO3	-28.3604	8.2946	-36.6551
CASO3.2H	-26.4796	-3.5984	-22.8812
CASO3.5H	-26.4742	-3.1245	-23.3498
BASO3	-29.8571	-5.5408	-24.3163
CH4(GAS)	-107.5520	-43.4486	-64.1034
CO2(GAS)	-25.1591	-18.1806	-6.9786
O2(GAS)	41.1928	88.4252	-47.2324

STEP NUMBER 1

9.0000-03 MOLES OF REACTION HAVE BEEN ADDED.

REACTION IS:

-1.00 MOLES OF N

VALENCE = 4.000

TOTAL MOLALITIES OF ELEMENTS

ELEMENT	MOLALITY	LOG MOLALITY
BA	9.2778020-06	-5.0326
BR	1.0588680-04	-3.9752
TOT ALK	3.2655490-02	-1.4860
CA	3.9421770-02	-1.4043
CL	2.3002190-01	-.6382
F	8.0483410-05	-4.0943
K	1.3816850-02	-1.8596
N	5.2749930-03	-2.2778
NA	1.7558690-01	-.7555
S	1.2733960-03	-2.8950
SI	6.4705280-04	-3.1891
SR	6.0729450-05	-4.2166

---- LOOK MIN IAP ----

PHASE	LOG IAP	LOG KT	LOG IAP/KT
ANHYDRIT	-5.8130	-4.4936	-1.3194
ARAGONIT	-4.8268	-8.2107	3.3839
BAF2	-14.0579	-5.7988	-8.2591
BARITE	-9.2654	-10.2238	.9584
CALCITE	-4.8268	-8.4064	3.5796
CELESTIT	-8.4495	-6.4518	-1.9977
CHALCEDO	-3.4008	-3.6990	.2982
CRISTOBA	-3.4008	-3.8036	.4028
FLUORITE	-10.6055	-11.1429	.5373
GYPSUM	-5.8202	-4.8601	-.9601
HALITE	-1.7056	1.5443	-3.2499
MAGADIIT	-14.7110	-14.3000	-.4110
MIRABILI	-5.5424	-1.8474	-3.6951
NATRON	-4.5562	-1.9212	-2.6350
QUARTZ	-3.4008	-4.2515	.8507
SI02(A,6	-3.4008	-2.8523	-.5485
SI02(A,P	-3.4008	-2.8523	-.5485
SRF2	-13.2420	-8.5885	-4.6535
STRONTIA	-7.4632	-9.2232	1.7600
THENARDI	-5.5068	-.1579	-5.3490
THERMONA	-4.5241	.2387	-4.7629
WITHERIT	-8.2792	-8.6040	.3248
SULFUR	-77.7806	-37.9421	-39.8385
LIME	17.9150	34.5962	-16.6812
PORTLAND	17.9114	23.8617	-5.9502
WOLLASTO	14.5142	13.7572	.7570
P-WOLLST	14.5142	14.6681	-.1539
CA-OLIVI	32.4292	39.7736	-7.3444
LARNITE	32.4292	41.3626	-8.9334
CASSIOS	50.3442	77.9987	-27.6545
NA2SO3	-23.5244	5.0649	-28.5893
K2SO3	-25.7865	8.2946	-34.0812
CASO3.2H	-23.8377	-3.5984	-20.2393
CASO3.5H	-23.8323	-3.1245	-20.7079
BASO3	-27.2830	-5.5408	-21.7421
CH4(GAS)	-94.8190	-43.4486	-51.3704
CO2(GAS)	-22.7418	-18.1806	-4.5612
O2(GAS)	36.0351	88.4252	-52.3901

TOTAL MOLALITIES OF ELEMENTS

ELEMENT	MOLALITY	LOG MOLALITY
BA	9.277802D-06	-5.0326
BR	1.058868D-04	-3.9752
C	3.265549D-02	-1.4860
CA	3.942177D-02	-1.4043
CL	2.300219D-01	-.6382
F	8.048341D-05	-4.0943
K	1.381685D-02	-1.8596
N	5.274993D-03	-2.2778
NA	1.755869D-01	-.7555
S	1.273396D-03	-2.8950
SI	6.470528D-04	-3.1891
SR	6.072945D-05	-4.2166

----DESCRIPTION OF SOLUTION----

PH = 10.0105
PE = -1.0000
ACTIVITY H2O = .9918
IONIC STRENGTH = .2777
TEMPERATURE = 10.0000
ELECTRICAL BALANCE = -1.6415D-02
THOR = -9.8776D+00
TOTAL ALKALINITY = 5.7315D-02
ITERATIONS = 18

 DISTRIBUTION OF SPECIES

I	SPECIES	Z	MOLALITY	LOG MOLALITY	ACTIVITY	LOG ACTIVITY	GAMMA	LOG GAMMA
1	H+	1.0	1.31839D-10	-9.8800	9.76016D-11	-10.0105	7.40306D-01	-.1306
2	E-	-1.0	1.00000D+01	1.0000	1.00000D+01	1.0000	1.00000D+00	.0000
3	H2O	.0	9.91843D-01	-.0036	9.91843D-01	-.0036	1.00000D+00	.0000
8	BA 2+	2.0	9.27737D-06	-5.0326	2.78657D-06	-5.5549	3.00362D-01	-.5224
9	BR-	-1.0	1.05887D-04	-3.9752	7.83886D-05	-4.1057	7.40306D-01	-.1306
10	CO3 2-	-2.0	6.28218D-03	-2.2019	1.88693D-03	-2.7242	3.00362D-01	-.5224
11	CA 2+	2.0	2.33954D-02	-1.6309	7.89698D-03	-2.1025	3.37544D-01	-.4717
13	CL-	-1.0	2.30022D-01	-.6382	1.55788D-01	-.8075	6.77277D-01	-.1692
16	F-	-1.0	7.56981D-05	-4.1209	5.60398D-05	-4.2515	7.40306D-01	-.1306
19	K+	1.0	1.38037D-02	-1.8600	9.34894D-03	-2.0292	6.77277D-01	-.1692
23	NO3 -	-1.0	2.99056D-37	-36.5242	2.21393D-37	-36.6548	7.40306D-01	-.1306
24	NA+	1.0	1.72480D-01	-.7633	1.26425D-01	-.8982	7.32982D-01	-.1349
29	SO4 2-	-2.0	8.38564D-04	-3.0765	1.94759D-04	-3.7105	2.32253D-01	-.6340
30	H4SiO4	.0	3.66705D-04	-3.4357	3.90917D-04	-3.4079	1.06603D+00	.0278
31	SR 2+	2.0	6.07249D-05	-4.2166	1.82395D-05	-4.7390	3.00362D-01	-.5224
55	NH4 +	1.0	5.26179D-03	-2.2789	3.89534D-03	-2.4095	7.40306D-01	-.1306
56	NO2 -	-1.0	5.33795D-25	-24.2726	3.95172D-25	-24.4032	7.40306D-01	-.1306
58	SO3 2-	-2.0	1.80687D-25	-24.7431	5.42716D-26	-25.2654	3.00362D-01	-.5224
65	OH-	-1.0	4.18218D-05	-4.3786	3.09610D-05	-4.5092	7.40306D-01	-.1306
66	H3SiO4 -	-1.0	2.78293D-04	-3.5555	2.06022D-04	-3.6861	7.40306D-01	-.1306
67	H2SiO4--	-2.0	2.05452D-06	-5.6873	6.17101D-07	-6.2096	3.00362D-01	-.5224
75	NH4SO4 -	-1.0	1.32015D-05	-4.8794	9.77319D-06	-5.0100	7.40306D-01	-.1306
84	CAOH +	1.0	7.45861D-06	-5.1273	5.52166D-06	-5.2579	7.40306D-01	-.1306
85	CAHCO3 +	1.0	3.95974D-04	-3.4023	2.93142D-04	-3.5329	7.40306D-01	-.1306
86	CACO3 AQ	.0	1.53616D-02	-1.8136	1.63758D-02	-1.7858	1.06603D+00	.0278
87	CASO4 AQ	.0	2.57699D-04	-3.5889	2.74714D-04	-3.5611	1.06603D+00	.0278
91	CAF +	1.0	3.70744D-06	-5.4309	2.74464D-06	-5.5615	7.40306D-01	-.1306
92	NACO3 -	-1.0	2.69260D-03	-2.5698	1.99335D-03	-2.7004	7.40306D-01	-.1306
93	NAHCO3 A	.0	2.62589D-04	-3.5807	2.79927D-04	-3.5530	1.06603D+00	.0278
94	NASO4 -	-1.0	1.50810D-04	-3.8216	1.11646D-04	-3.9522	7.40306D-01	-.1306
96	NAF AQ	.0	1.07785D-06	-5.9674	1.14902D-06	-5.9397	1.06603D+00	.0278
97	KSO4 -	-1.0	1.31215D-05	-4.8820	9.71390D-06	-5.0126	7.40306D-01	-.1306
134	SROH +	1.0	4.54739D-09	-8.3422	3.36646D-09	-8.4728	7.40306D-01	-.1306
135	BAOH +	1.0	4.35034D-10	-9.3615	3.22059D-10	-9.4921	7.40306D-01	-.1306
272	HCO3 -	-1.0	7.65909D-03	-2.1158	5.67007D-03	-2.2464	7.40306D-01	-.1306
273	H2CO3 AQ	.0	1.50572D-06	-5.8223	1.60513D-06	-5.7945	1.06603D+00	.0278
274	HSO4 -	-1.0	1.66147D-12	-11.7795	1.23000D-12	-11.9101	7.40306D-01	-.1306
275	HF AQ	.0	5.55696D-12	-11.2552	5.92387D-12	-11.2274	1.06603D+00	.0278
276	HF2 -	-1.0	1.54656D-15	-14.8106	1.14493D-15	-14.9412	7.40306D-01	-.1306
277	H2F2 AQ	.0	1.64490D-22	-21.7839	1.75350D-22	-21.7561	1.06603D+00	.0278
353	HSO3-	-1.0	1.05905D-28	-27.9751	7.84023D-29	-28.1057	7.40306D-01	-.1306

PAGE 7
 0030011000 1 2 .00000
 REACTION
 13 -1.000 -1.000 24 -1.000 1.000
 STEPS
 .130
 STEP NUMBER 1

1.300D-01 MOLES OF REACTION HAVE BEEN ADDED.

REACTION IS:

-1.00 MOLES OF CL VALENCE = -1.000
 -1.00 MOLES OF NA VALENCE = 1.000

TOTAL MOLALITIES OF ELEMENTS

ELEMENT	MOLALITY	LOG MOLALITY
BA	9.277802D-06	-5.0326
BR	1.058868D-04	-3.9752
C	3.265549D-02	-1.4860
CA	3.942177D-02	-1.4043
CL	1.000219D-01	-.9999
F	8.048341D-05	-4.0943
K	1.381685D-02	-1.8596
N	5.274993D-03	-2.2778
NA	4.558691D-02	-1.3412
S	1.273396D-03	-2.8950
SI	6.470528D-04	-3.1891
SR	6.072945D-05	-4.2166

---- LOOK MIN IAP ----

PHASE	LOG IAP	LOG KT	LOG IAP/KT
ANHYDRIT	-5.6811	-4.4936	-1.1875
ARAGONIT	-4.7791	-8.2107	3.4316
BAF2	-13.9593	-5.7988	-8.1604
BARITE	-9.0866	-10.2238	1.1373
CALCITE	-4.7791	-8.4064	3.6274
CELESTIT	-8.2707	-6.4518	-1.8189
CHALCEDO	-3.4098	-3.6990	.2892
CRISTOBA	-3.4098	-3.8036	.3938
FLUORITE	-10.5538	-11.1429	.5891
GYPSUM	-5.6843	-4.8601	-.8242
HALITE	-2.6002	1.5443	-4.1445
MAGADIIT	-15.3219	-14.3000	-1.0219
MIRABILI	-6.5393	-1.8474	-4.6919
NATRON	-5.6373	-1.9212	-3.7161
QUARTZ	-3.4098	-4.2515	.8417
SI02(A,G	-3.4098	-2.8523	-.5575
SI02(A,P	-3.4098	-2.8523	-.5575
SRF2	-13.1433	-8.5885	-4.5548
STRONTIA	-7.3686	-9.2232	1.8546
THENARDI	-6.5230	-.1579	-6.3651
THERMONA	-5.6226	.2387	-5.8614
WITHERIT	-8.1846	-8.6040	.4194
SULFUR	-77.7461	-37.9421	-39.8040

-----LOOK MIN IAP Cont'd-----

PHASE	LOG IAP	LOG KT	LOG IAP/KT
LIME	17.9500	34.5962	-16.6462
PORTLAND	17.9484	23.8617	-5.9132
WOLLASTO	14.5402	13.7572	.7831
P-WOLLST	14.5402	14.6681	-.1279
CA-OLIVI	32.4903	39.7736	-7.2833
LARNITE	32.4903	41.3626	-8.8723
CA3SI05	50.4403	77.9987	-27.5584
NA2SO3	-24.5613	5.0649	-29.6263
K2SO3	-25.6219	8.2946	-33.9165
CAS03.2H	-23.7226	-3.5984	-20.1242
CAS03.5H	-23.7202	-3.1245	-20.5957
BAS03	-27.1249	-5.5408	-21.5841
CH4(GAS)	-94.8856	-43.4486	-51.4371
CO2(GAS)	-22.7291	-18.1806	-4.5485
O2(GAS)	36.0766	88.4252	-52.3486

TOTAL MOLALITIES OF ELEMENTS

ELEMENT	MOLALITY	LOG MOLALITY
BA	9.277802D-06	-5.0326
BR	1.058868D-04	-3.9752
C	3.265549D-02	-1.4860
CA	3.942177D-02	-1.4043
CL	1.000219D-01	-.9999
F	8.048341D-05	-4.0943
K	1.381685D-02	-1.8596
N	5.274993D-03	-2.2778
NA	4.558691D-02	-1.3412
S	1.273396D-03	-2.8950
SI	6.470528D-04	-3.1891
SR	6.072945D-05	-4.2166

-----DESCRIPTION OF SOLUTION-----

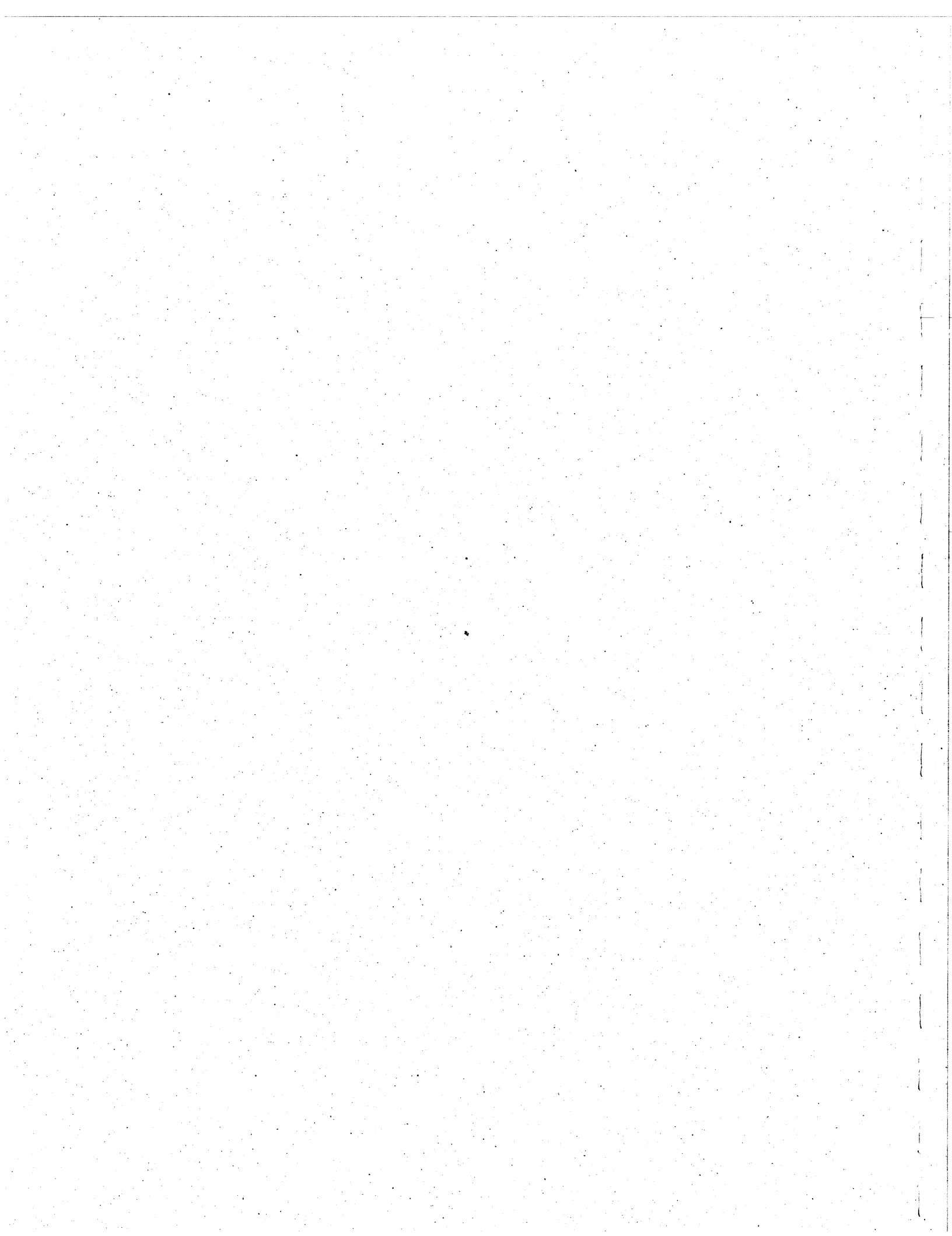
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PE = -1.0000
ACTIVITY H2O = .9963
IONIC STRENGTH = .1422
TEMPERATURE = 10.0000
ELECTRICAL BALANCE = -1.6415D-02
THOR = -9.8776D+00
TOTAL ALKALINITY = 5.7314D-02
ITERATIONS = 18

 DISTRIBUTION OF SPECIES

I	SPECIES	Z	MOLALITY	LOG MOLALITY	ACTIVITY	LOG ACTIVITY	GAMMA	LOG GAMMA
1	H+	1.0	1.24547D-10	-9.9047	9.55057D-11	-10.0200	7.66826D-01	-.1153
2	E-	-1.0	1.00000D+01	1.0000	1.00000D+01	1.0000	1.00000D+00	.0000
3	H2O	.0	9.96267D-01	-.0016	9.96267D-01	-.0016	1.00000D+00	.0000
8	BA 2+	2.0	9.27731D-06	-5.0326	3.20781D-06	-5.4938	3.45769D-01	-.4612
9	BR-	-1.0	1.05887D-04	-3.9752	8.11967D-05	-4.0905	7.66826D-01	-.1153
10	CO3 2-	-2.0	5.89414D-03	-2.2296	2.03801D-03	-2.6908	3.45769D-01	-.4612
11	CA 2+	2.0	2.09436D-02	-1.6789	8.16060D-03	-2.0883	3.89646D-01	-.4093
13	CL-	-1.0	1.00022D-01	-.9999	7.32591D-02	-1.1351	7.32430D-01	-.1352
16	F-	-1.0	7.63067D-05	-4.1174	5.85139D-05	-4.2327	7.66826D-01	-.1153
19	K+	1.0	1.37989D-02	-1.8602	1.01067D-02	-1.9954	7.32430D-01	-.1352
23	NO3 -	-1.0	3.76260D-37	-36.4245	2.88526D-37	-36.5398	7.66826D-01	-.1153
24	NA+	1.0	4.46962D-02	-1.3497	3.42683D-02	-1.4651	7.66694D-01	-.1154
29	SO4 2-	-2.0	8.26121D-04	-3.0830	2.55388D-04	-3.5928	3.09141D-01	-.5098
30	H4SiO4	.0	3.73877D-04	-3.4273	3.86317D-04	-3.4131	1.03327D+00	.0142
31	SR 2+	2.0	6.07243D-05	-4.2166	2.09966D-05	-4.6779	3.45769D-01	-.4612
55	NH4 +	1.0	5.25770D-03	-2.2792	4.03174D-03	-2.3945	7.66826D-01	-.1153
56	NO2 -	-1.0	6.40210D-25	-24.1937	4.90930D-25	-24.3090	7.66826D-01	-.1153
58	SO3 2-	-2.0	1.96201D-25	-24.7073	6.78402D-26	-25.1685	3.45769D-01	-.4612
65	OH-	-1.0	4.14456D-05	-4.3825	3.17815D-05	-4.4978	7.66826D-01	-.1153
66	H3SiO4 -	-1.0	2.71334D-04	-3.5665	2.08066D-04	-3.6818	7.66826D-01	-.1153
67	H2SiO4--	-2.0	1.84198D-06	-5.7347	6.36899D-07	-6.1959	3.45769D-01	-.4612
75	NH4SO4 -	-1.0	1.72977D-05	-4.7620	1.32643D-05	-4.8773	7.66826D-01	-.1153
84	CAOH +	1.0	7.63826D-06	-5.1170	5.85721D-06	-5.2323	7.66826D-01	-.1153
85	CAHCO3 +	1.0	4.17509D-04	-3.3793	3.20156D-04	-3.4946	7.66826D-01	-.1153
86	CACO3 AQ	.0	1.76889D-02	-1.7523	1.82774D-02	-1.7381	1.03327D+00	.0142
87	CASO4 AQ	.0	3.60271D-04	-3.4434	3.72258D-04	-3.4292	1.03327D+00	.0142
91	CAF +	1.0	3.86200D-06	-5.4132	2.96148D-06	-5.5285	7.66826D-01	-.1153
92	NACO3 -	-1.0	7.61025D-04	-3.1186	5.83573D-04	-3.2339	7.66826D-01	-.1153
93	NAHCO3 A	.0	7.76093D-05	-4.1101	8.01916D-05	-4.0959	1.03327D+00	.0142
94	NASO4 -	-1.0	5.17498D-05	-4.2861	3.96830D-05	-4.4014	7.66826D-01	-.1153
96	NAF AQ	.0	3.14729D-07	-6.5021	3.25201D-07	-6.4878	1.03327D+00	.0142
97	KSO4 -	-1.0	1.79576D-05	-4.7458	1.37703D-05	-4.8611	7.66826D-01	-.1153
134	SROH +	1.0	5.18769D-09	-8.2850	3.97805D-09	-8.4003	7.66826D-01	-.1153
135	BAOH +	1.0	4.96291D-10	-9.3043	3.80569D-10	-9.4196	7.66826D-01	-.1153
272	HCO3 -	-1.0	7.81475D-03	-2.1071	5.99255D-03	-2.2224	7.66826D-01	-.1153
273	H2CO3 AQ	.0	1.60654D-06	-5.7941	1.66000D-06	-5.7799	1.03327D+00	.0142
274	HSO4 -	-1.0	2.05817D-12	-11.6865	1.57826D-12	-11.8018	7.66826D-01	-.1153
275	HF AQ	.0	5.85767D-12	-11.2323	6.05258D-12	-11.2181	1.03327D+00	.0142
276	HF2 -	-1.0	1.59287D-15	-14.7978	1.22145D-15	-14.9131	7.66826D-01	-.1153
277	H2F2 AQ	.0	1.77158D-22	-21.7516	1.83053D-22	-21.7374	1.03327D+00	.0142
353	HSO3-	-1.0	1.25060D-28	-27.9029	9.58993D-29	-28.0182	7.66826D-01	-.1153

Appendix C

Assessment of Metal Solubilities



APPENDIX C

METAL SOLUBILITY

A modelling exercise was conducted to evaluate the maximum concentrations of various metals that might potentially occur in the leachate. These metals included zinc, aluminum, lead, iron and nickel.

Discussion of the modelling process

The modelling was based upon the geochemical model PHREEQE developed by the United States Geological Survey (Parkhurst et al., 1985). As input, the model requires an estimate of the pH, pe (redox potential), major ion concentrations and trace element concentrations. These input were taken from the predicted landfill leachate concentrations (Table 3, Column E) for the proposed East Quarry Landfill. The overall composition of the leachate is not critical, except that:

- a) it must be a complex fluid to facilitate full speciation;
- b) the pH of the leachate has been predicted to remain highly alkaline (greater than 10). pHs between 7 and 12 were considered for this exercise. This is critical for the selection appropriate solid phases used to model maximum concentrations (as discussed further below); and
- c) the redox potential of the leachate is estimated to be reducing (pe = -1). The redox potential is important because the solubility for some metals varies greatly with valence.

The predicted leachate included estimated concentrations for barium, bromide, bicarbonate, calcium, chloride, fluoride, potassium, nitrogen, sodium, sulphate, silica and strontium. Species interaction between metal phases is assumed to be negligible.

To estimate soluble limits for the metals, phases were selected for modelling from the available PHREEQE thermodynamic database (about 400 solid phases). Preference was given to reduced oxides, hydroxides, carbonates and pure metals because these phases are most likely to present within the waste and are stable under reducing, alkaline conditions. The following phases were selected for equilibration:

aluminum: amorphous Al(OH)₃
zinc: Zn(OH)₂
iron: ferrihydrite
nickel: Ni(OH)₂
lead: Pb(OH)₂

Solubilities were determined by individually dissolving these phases until equilibration with the predicted leachate quality at unit pHs between 7 and 12 inclusive. The initial solution was charge balanced using calcium and chloride. Equilibration was conducted under closed conditions at a pe of -1 and a temperature of 10°C. Resulting concentrations were then converted into units of mg/L and plotted.

General Conclusions

Metal concentrations are expected to be low in the leachate because of the physical limits imposed by thermodynamic conditions.

Under the alkaline conditions predicted for the leachate, these metals exhibit low solubility that decreases with increasing pH (except for aluminum). The accompanying figures demonstrate these relationships.

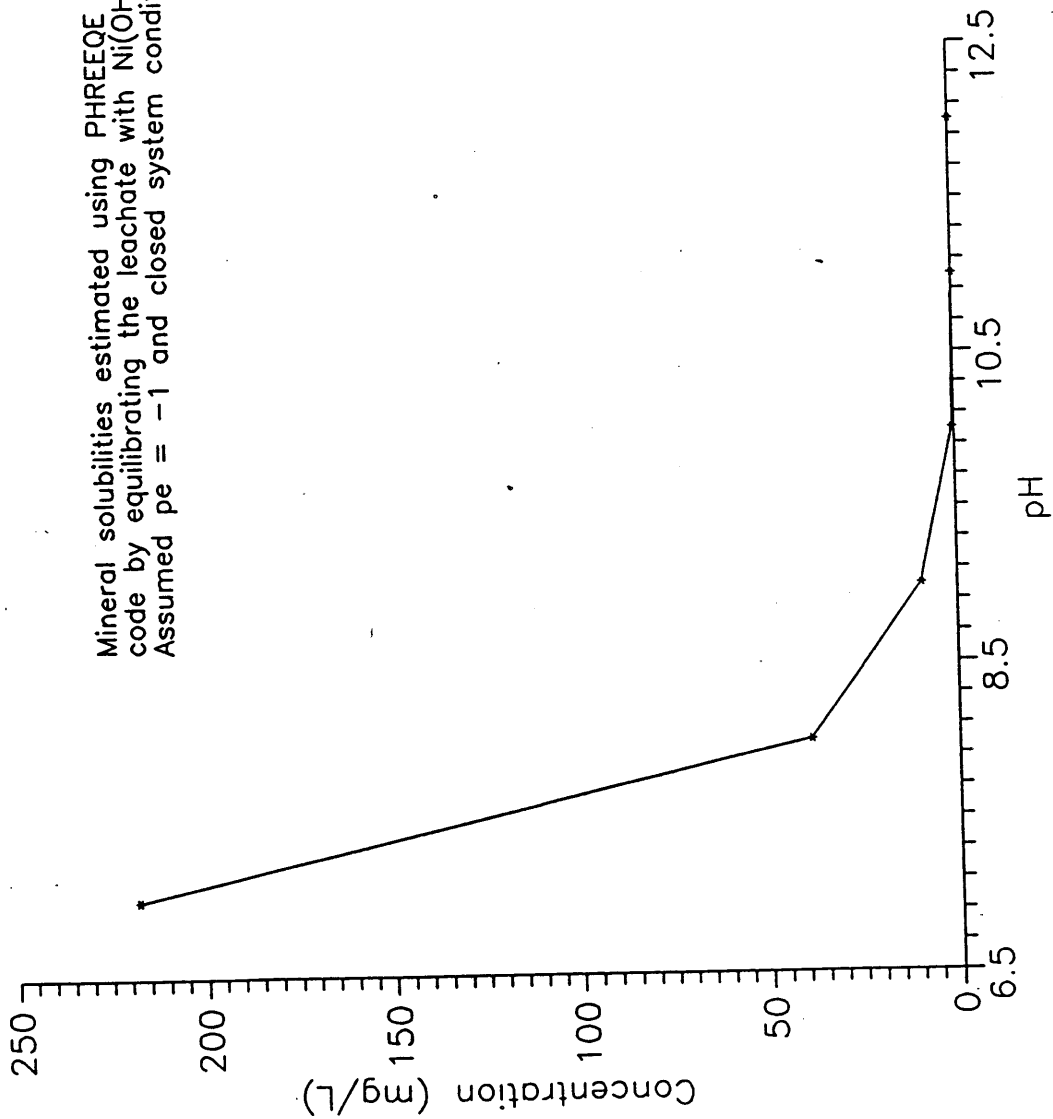
Sensitivity Analyses

Further examinations of ZnO, Zn metal, ZnSO₄ and ZnCO₃ were completed to evaluate the effects of oxides, carbonates, sulphates and pure metal. The metal and sulphate phases were found to have much higher solubilities than the oxides and hydroxides (although the kinetics of these dissolution reactions would prevent equilibrium from being reached). ZnO constrains the maximum concentrations under slightly alkaline conditions and ZnCO₃ limits the concentrations under neutral and slightly acidic conditions. Similar behavior is expected for nickel, aluminum and iron.

The redox sensitivity was not established. It is expected that this exercise is valid for reducing conditions but is not valid for oxidizing conditions.

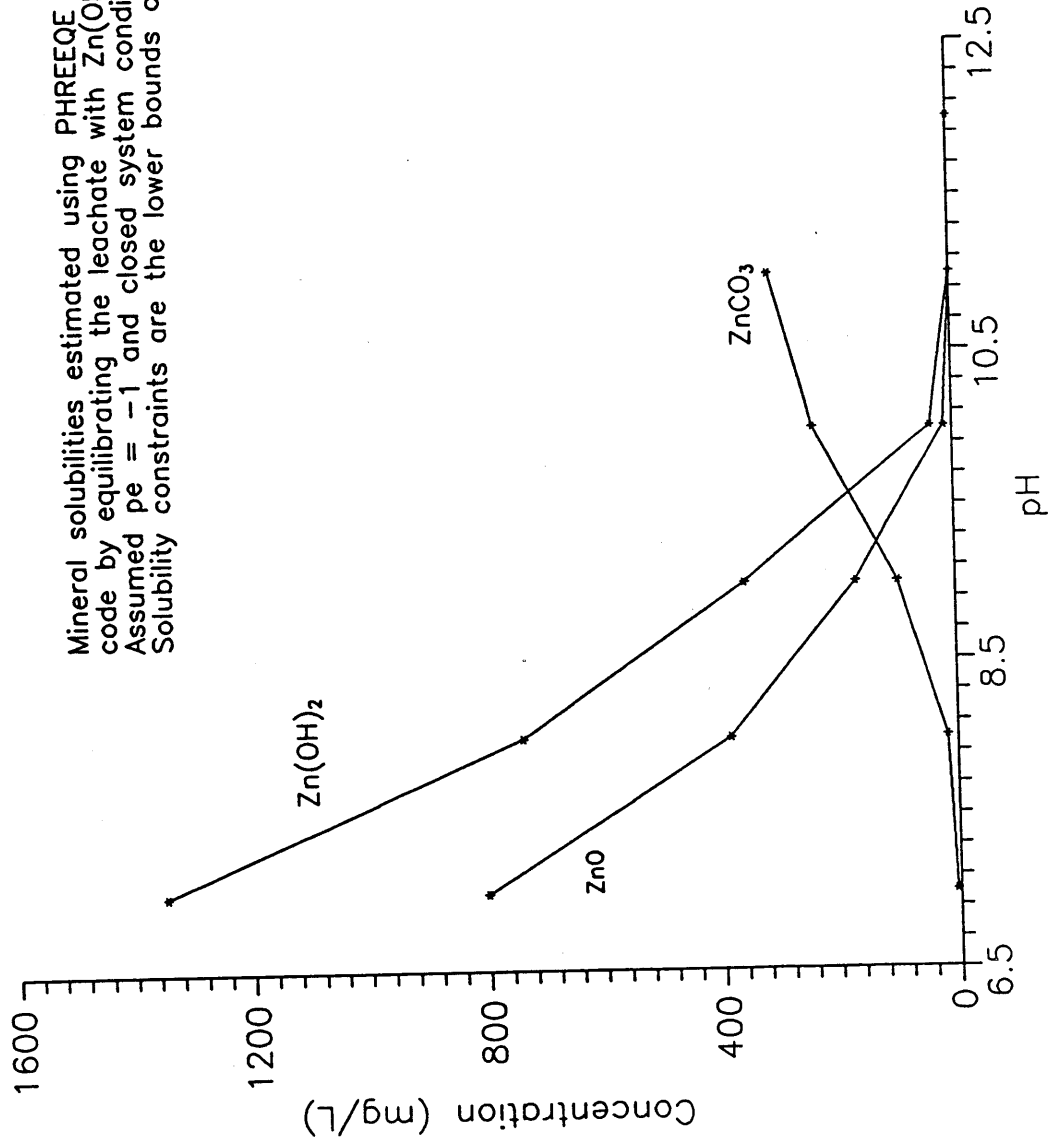
Theoretical nickel maximum concentrations

Mineral solubilities estimated using PHREEQE geochemical code by equilibrating the leachate with $\text{Ni}(\text{OH})_2$. Assumed $p_e = -1$ and closed system conditions prevail.



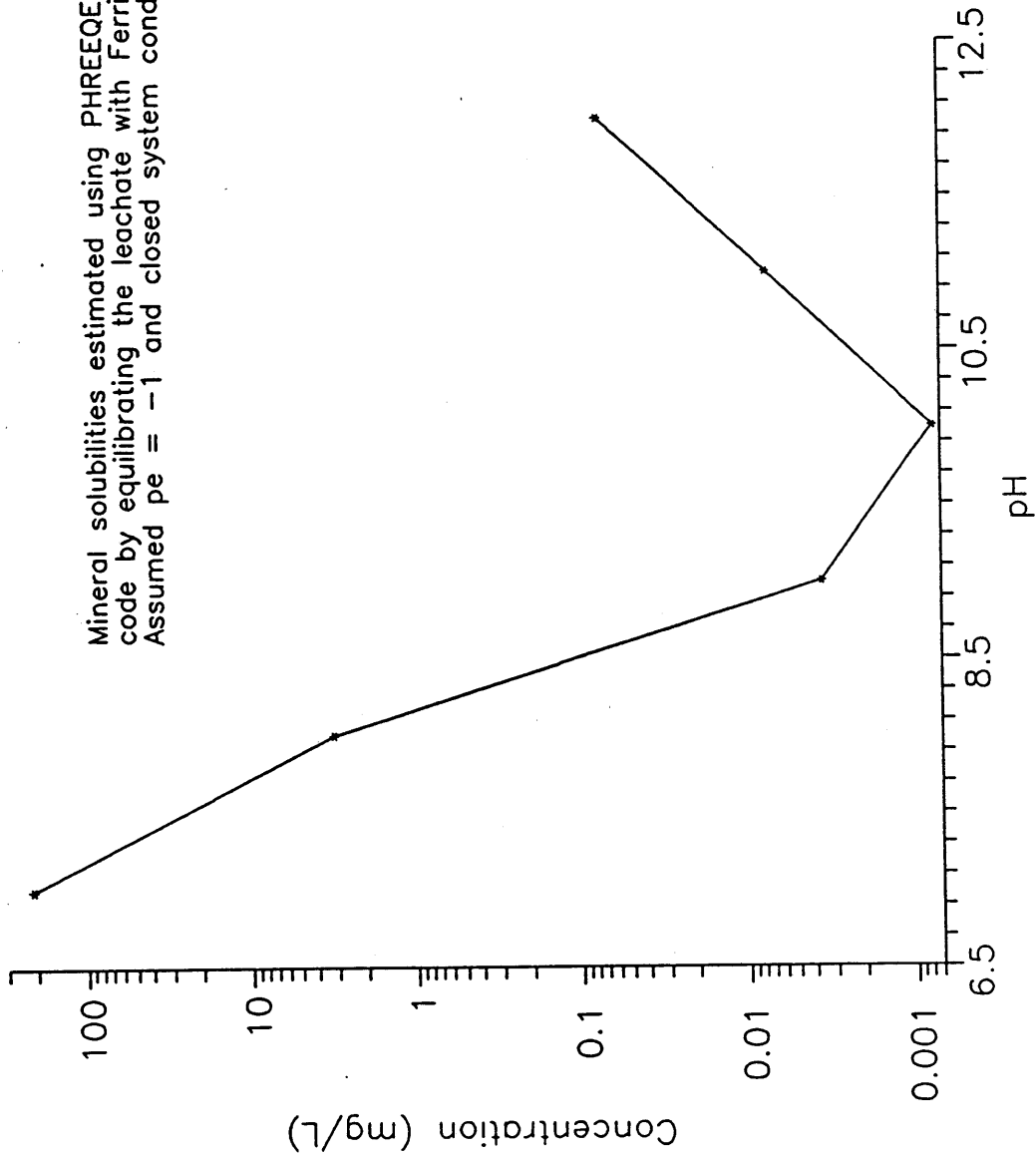
Theoretical zinc maximum concentrations

Mineral solubilities estimated using PHREEQE geochemical code by equilibrating the leachate with $Zn(OH)_2$, $ZnCO_3$ and ZnO . Assumed $pe = -1$ and closed system conditions prevail. Solubility constraints are the lower bounds of each line.



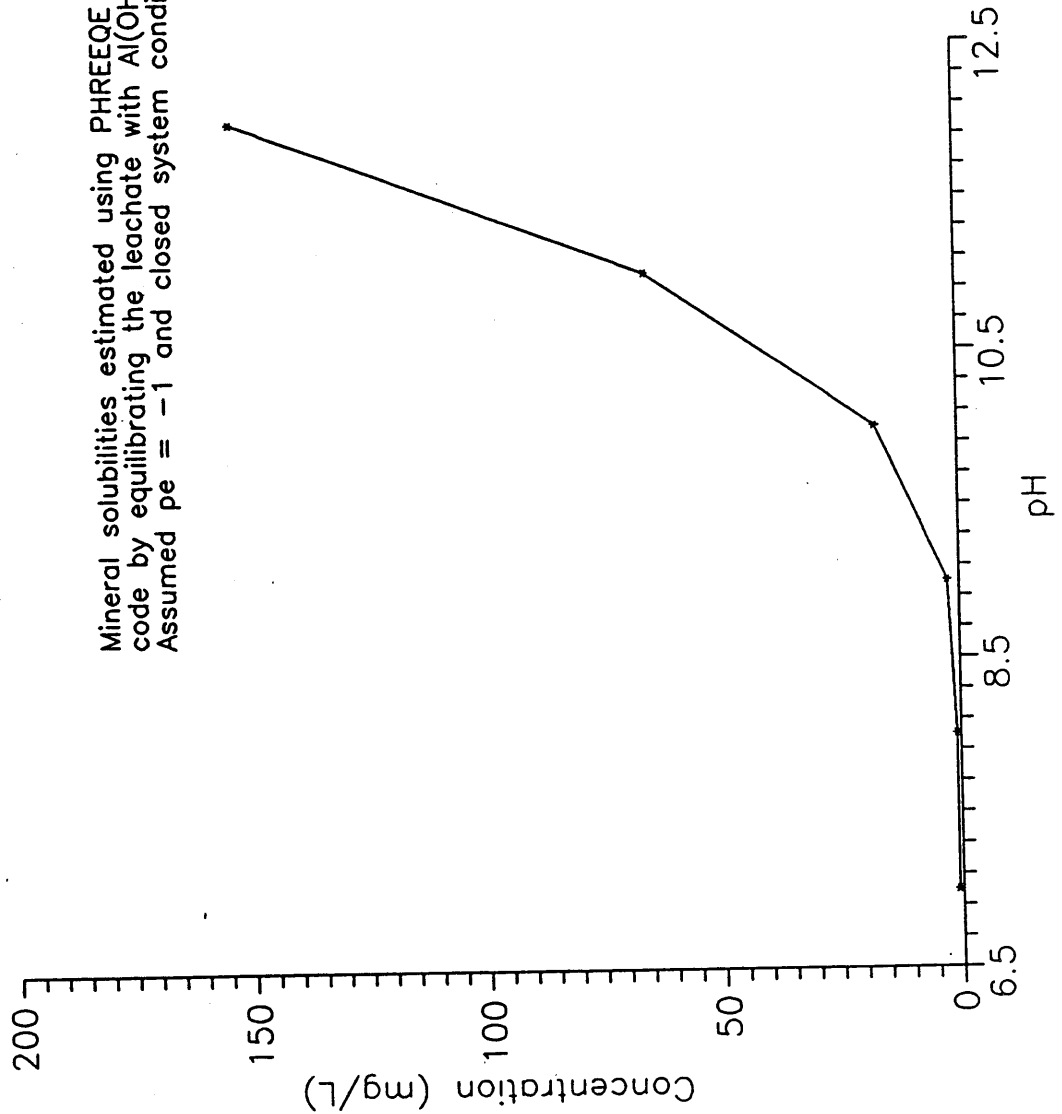
Theoretical iron maximum concentrations

Mineral solubilities estimated using PHREEQE geochemical code by equilibrating the leachate with Ferrihydrite. Assumed $p_e = -1$ and closed system conditions prevail.



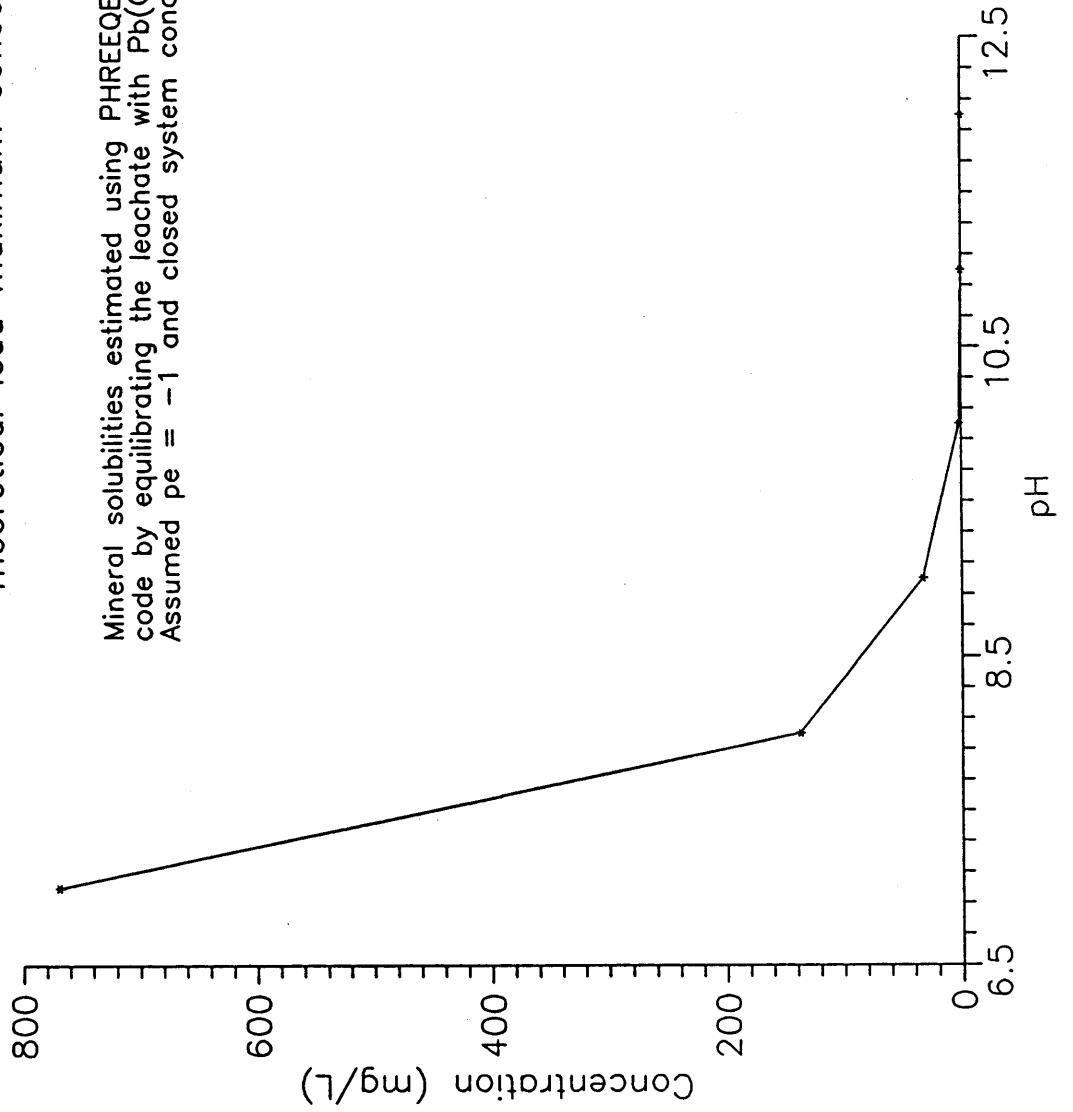
Theoretical aluminum maximum concentrations

Mineral solubilities estimated using PHREEQE geochemical code by equilibrating the leachate with $Al(OH)_3$.
Assumed $pe = -1$ and closed system conditions prevail.



Theoretical lead maximum concentrations

Mineral solubilities estimated using PHREEQE geochemical code by equilibrating the leachate with $Pb(OH)_2$.
Assumed $pe = -1$ and closed system conditions prevail.



Appendix D

Critical Contaminant Assessment

Table D1: Inorganic Parameters

Table D2: Organic Parameters

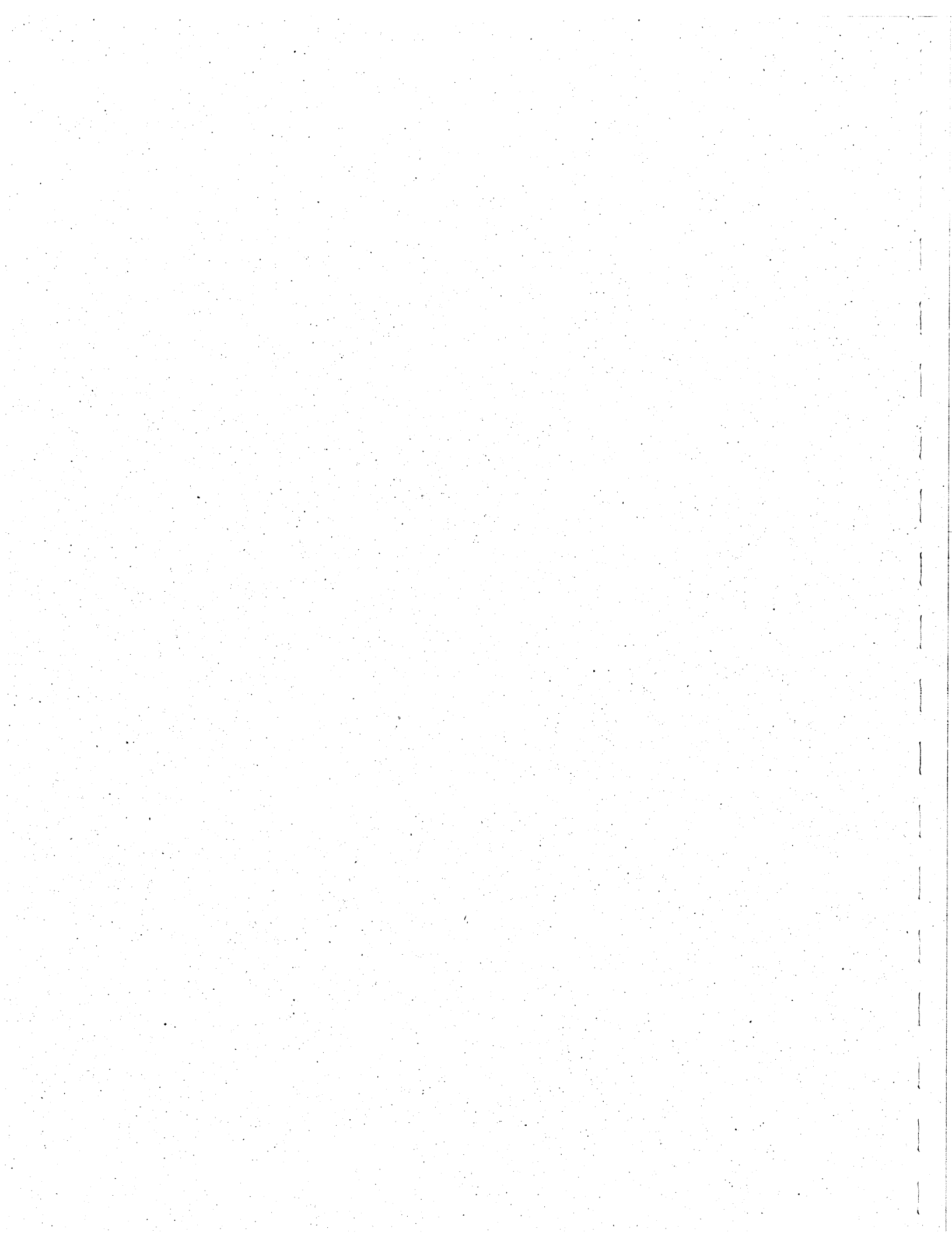


TABLE D1: Assessment of Critical Contaminants

West Quarry Leachate

Compound		ODWO		Predicted East Quarry Landfill Leachate	West Quarry Leachate (range in all monitors)	
units					Range	Average
					Total # samples 78	
pH	pH units	6.5-8.5	o	7.4 - 12.83	7.4 - 12.83	10.86
Conductivity	µmhos/cm			814 - 12750	814 - 134000	13171
TDS	mg/L	500	a	598 - 14256	598 - 118000	10445
COD	mg/L			800 - 5000	10 - 5000	649
TOC	mg/L			154 - 1310	4.6 - 1310	185
Alkalinity	mg CaCO ₃ /L	30-500	o	232 - 4550	49 - 8440	1582
Hardness	mg CaCO ₃ /L	80-100	o	109 - 2552	70 - 4552	1329
Calcium	mg/L			343 - 1820	20.6 - 1820	523.5
Magnesium	mg/L			0 - 26.4	0 - 26.4	4.6
Sodium	mg/L	200	a	161 - 739	139 - 47600	2594
Potassium	mg/L			1550 - 2360	15.1 - 2360	373
Chloride	mg/L	250	a	34 - 161	0 - 87000	4547
Fluoride	mg/L	1.5	h	0 - 3.9	0 - 4.2	2
Bromide	mg/L			0 - 78	0 - 78	7
Sulphate	mg/L	500	a	715 - 3180	0 - 3180	619
Ammonia	mg/L			3 - 31	3.76 - 2330	154
TKN	mg/L			51 - 110	5.4 - 2330	167
Nitrate	mg/L	10	h	0	0 - 68.7	0.90
Nitrite	mg/L	1	h	0.01 - 0.029	0 - 0.290	0.007
Phosphate	mg/L			0 - 1.7	0 - 2.00	0.23
Aluminum	mg/L	0.1	o	0 - 0.58	0 - 3.41	0.17
Barium	mg/L	1	h	0.05 - 2.07	0.03 - 2.07	0.432
Beryllium	mg/L			0 - 0.001	0 - 0.0014	0.0001
Boron	mg/L	5	h	0 - 0.627	0 - 1.24	0.29
Cadmium	mg/L	0.005	h	0 - 0.001	0 - 0.0008	0.00002
Chromium	mg/L	0.05	h	0 - 0.02	0 - 0.04	0.002
Cobalt	mg/L			0 - 0.15	0 - 0.16	0.01
Copper	mg/L	1	a	0 - 0.15	0 - 0.15	0.01
Lead	mg/L	0.01	h	0 - 0.04	0 - 0.04	0.001
Iron	mg/L	0.3	a	0 - 0.63	0 - 0.63	0.07
Manganese	mg/L	0.05	a	0 - 0.44	0 - 0.44	0.03
Molybdenum	mg/L			0 - 1.1	0 - 1.1	0.11
Nickel	mg/L			0 - 0.78	0 - 0.78	0.14
Silica	mg/L			7.17 - 37.3	1.9 - 37.3	6.94
Silver	mg/L			0	0 - 0.006	0.0002
Strontium	mg/L			2.41 - 10.9	0.47 - 10.9	2.91
Titanium	mg/L			0 - 0.011	0 - 0.017	0.003
Vanadium	mg/L			0 - 0.07	0 - 0.07	0.01
Zinc	mg/L	5	a	0 - 0.9	0 - 0.5	0.02
Thorium	mg/L				0 - 0.14	0.02
Zircon	mg/L				0 - 0.04	0.01
Phenols	µg/L			180 - 47500	180 - 47500	7000

h - health related objective
a - aesthetic objective associated with taste, smell and colour
o - operational objective to ensure efficient treatment of water

TABLE D1: Assessment of Critical Contaminants

Eramosa Dolostone

Compound		ODWO		Predicted East Quarry Landfill Leachate		Background Range in Eramosa Dolostone		Reasonable Use
units						Range	Average	
						Total # Samples 93		Based on average
pH	pH units	6.5-8.5	o	7.4 - 12.83	7.11 - 8.6	7.49	Eramosa	
Conductivity	µmhos/cm			814 - 12750	617 - 5750	2226		
TDS	mg/L	500	a	598 - 14256	443 - 12560	2136	2136	
COD	mg/L			800 - 5000	0 - 552	29.72		
TOC	mg/L			154 - 1310	0.6 - 35.3	6.01		
Alkalinity	mg CaCO ₃ /L	30-500	o	232 - 4550	177 - 547	375	438	
Hardness	mg CaCO ₃ /L	80-100	o	109 - 2552	358.9 - 4746	1301	1301	
Calcium	mg/L			343 - 1820	96.3 - 533	237		
Magnesium	mg/L			0 - 26.4	27.4 - 896	172		
Sodium	mg/L	200	a	161 - 739	0 - 260	90	145	
Potassium	mg/L			1550 - 2360	0 - 37.3	3.47		
Chloride	mg/L	250	a	34 - 161	7.8 - 496	151	200	
Fluoride	mg/L	1.5	h	0 - 3.9	0 - 1.3	0.70	0.90	
Bromide	mg/L			0 - 78	0 - 1.9	0.05		
Sulphate	mg/L	500	a	715 - 3180	98.2 - 4940	904	904	
Ammonia	mg/L			3 - 31	0 - 0.77	0.13		
TKN	mg/L			51 - 110	0.02 - 2.6	0.45		
Nitrate	mg/L	10	h	0	0 - 19.2	0.96	3.22	
Nitrite	mg/L	1	h	0.01 - 0.029	0 - 0.21	0.01	0.25	
Phosphate	mg/L			0 - 1.7	0 - 1.3	0.06		
Aluminum	mg/L	0.1	o	0 - 0.58	0 - 0.67	0.05	0.07	
Barium	mg/L	1	h	0.05 - 2.07	0 - 0.099	0.04	0.28	
Beryllium	mg/L			0 - 0.001	0 - 0.003	0.0001		
Boron	mg/L	5	h	0 - 0.627	0 - 1.1	0.14	1.35	
Cadmium	mg/L	0.005	h	0 - 0.001	0 - 0.055	0.0011	0.002	
Chromium	mg/L	0.05	h	0 - 0.02	0 - 0.05	0.003	0.015	
Cobalt	mg/L			0 - 0.15	0 - 0.08	0.001		
Copper	mg/L	1	a	0 - 0.15	0 - 0.17	0.004	0.502	
Lead	mg/L	0.01	h	0 - 0.04	0 - 0.02	0.0005	0.003	
Iron	mg/L	0.3	a	0 - 0.63	0 - 3.28	0.24	0.269	
Manganese	mg/L	0.05	a	0 - 0.44	0 - 1.81	0.14	0.141	
Molybdenum	mg/L			0 - 1.1	0	0		
Nickel	mg/L			0 - 0.78	0 - 0.08	0.003		
Silica	mg/L			7.17 - 37.3	1.16 - 8.64	5.23		
Silver	mg/L			0	0 - 0.008	0.0004		
Strontium	mg/L			2.41 - 10.9	0.266 - 6.48	2.24		
Titanium	mg/L			0 - 0.011	0 - 0.011	0.0008		
Vanadium	mg/L			0 - 0.07	0 - 0.025	0.0018		
Zinc	mg/L	5	a	0 - 0.9	0 - 1.09	0.21	2.60	
Thorium	mg/L				0 - 0.07	0.01		
Zircon	mg/L				0 - 0.05	0.0040		
Phenols	µg/L			180 - 47500	0 - 2.0	0.09		

h - health related objective
a - aesthetic objective associated with taste, smell and colour
o - operational objective to ensure efficient treatment of water

TABLE D1: Assessment of Critical Contaminants

Vinemount Flow Zone

Compound		ODWO		Predicted East Quarry Landfill Leachate	Background Range in Vinemount Flow Zone		Reasonable Use
units					Range	Average	
					Total # Samples 107		Based on average
pH	pH units	6.5-8.5	o	7.4 - 12.83	6.92 - 8.73	7.52	VFZ
Conductivity	µmhos/cm			814 - 12750	330 - 4640	2513	
TDS	mg/L	500	a	598 - 14256	219 - 5410	2389	2389
COD	mg/L			800 - 5000	0 - 600	46	
TOC	mg/L			154 - 1310	1.2 - 26	7.39	
Alkalinity	mg CaCO ₃ /L	30-500	o	232 - 4550	52 - 503	269	384
Hardness	mg CaCO ₃ /L	80-100	o	109 - 2552	576.8 - 2428	1384	1384
Calcium	mg/L			343 - 1820	178 - 711	400	
Magnesium	mg/L			0 - 26.4	19.2 - 270	93	
Sodium	mg/L	200	a	161 - 739	8.3 - 512	119	160
Potassium	mg/L			1550 - 2360	0 - 47.7	14	
Chloride	mg/L	250	a	34 - 161	13.5 - 890	179	215
Fluoride	mg/L	1.5	h	0 - 3.9	0 - 1.3	0.79	0.97
Bromide	mg/L			0 - 78	0 - 9.2	0.82	
Sulphate	mg/L	500	a	715 - 3180	51.7 - 2700	1112	1112
Ammonia	mg/L			3 - 31	0 - 4.7	1.01	
TKN	mg/L			51 - 110	0.08 - 33	1.64	
Nitrate	mg/L	10	h	0	0 - 6.1	0.39	2.79
Nitrite	mg/L	1	h	0.01 - 0.029	0 - 0.15	0.01	0.25
Phosphate	mg/L			0 - 1.7	0 - 1.8	0.23	
Aluminum	mg/L	0.1	o	0 - 0.58	0 - 0.7	0.03	0.07
Barium	mg/L	1	h	0.05 - 2.07	0 - 0.091	0.025	0.27
Beryllium	mg/L			0 - 0.001	0 - 0.003	0.0001	
Boron	mg/L	5	h	0 - 0.627	0.07 - 7.2	0.95	1.96
Cadmium	mg/L	0.005	h	0 - 0.001	0 - 0.017	0.0005	0.002
Chromium	mg/L	0.05	h	0 - 0.02	0 - 0.04	0.005	0.016
Cobalt	mg/L			0 - 0.15	0 - 0.14	0.002	
Copper	mg/L	1	a	0 - 0.15	0 - 0.3	0.005	0.502
Lead	mg/L	0.01	h	0 - 0.04	0 - 0.02	0.0004	0.003
Iron	mg/L	0.3	a	0 - 0.63	0 - 2.07	0.15	0.225
Manganese	mg/L	0.05	a	0 - 0.44	0 - 5.33	0.53	0.534
Molybdenum	mg/L			0 - 1.1	0 - 0.3	0.005	
Nickel	mg/L			0 - 0.78	0 - 0.31	0.02	
Silica	mg/L			7.17 - 37.3	0.86 - 10.3	3.88	
Silver	mg/L			0	0 - 0.0002	0	
Strontium	mg/L			2.41 - 10.9	1.04 - 11.2	4.80	
Titanium	mg/L			0 - 0.011	0 - 0.02	0.002	
Vanadium	mg/L			0 - 0.07	0 - 0.138	0.005	
Zinc	mg/L	5	a	0 - 0.9	0 - 0.72	0.08	2.54
Thorium	mg/L				0 - 0.12	0.02	
Zircon	mg/L				0 - 0.04	0.003	
Phenols	µg/L			180 - 47500	0 - 250	2.56	

h - health related objective
a - aesthetic objective associated with taste, smell and colour
o - operational objective to ensure efficient treatment of water

TABLE D1: Assessment of Critical Contaminants

Upper Flow Zone

Compound		ODWO		Predicted East Quarry Landfill Leachate		Background Range in Upper Flow Zone		Reasonable Use
units						Range	Average	Based on average
						Total # Samples 23		
pH	pH units	6.5-8.5	o	7.4 - 12.83	7.16 - 8.3	7.52	UFZ	
Conductivity	µmhos/cm			814 - 12750	1259 - 9390	4114		
TDS	mg/L	500	a	598 - 14256	863 - 7331	3266	3266	
COD	mg/L			800 - 5000	0 - 330	61		
TOC	mg/L			154 - 1310	0.7 - 13	4.52		
Alkalinity	mg CaCO ₃ /L	30-500	o	232 - 4550	113 - 466	286	393	
Hardness	mg CaCO ₃ /L	80-100	o	109 - 2552	435.1 - 2151	1332	1332	
Calcium	mg/L			343 - 1820	127 - 633	383		
Magnesium	mg/L			0 - 26.4	28.3 - 144	91		
Sodium	mg/L	200	a	161 - 739	61.5 - 1490	473	473	
Potassium	mg/L			1550 - 2360	0 - 51.5	25		
Chloride	mg/L	250	a	34 - 161	86.3 - 2500	689	689	
Fluoride	mg/L	1.5	h	0 - 3.9	0.2 - 8.5	1.01	1.13	
Bromide	mg/L			0 - 78	0 - 6.4	1.56		
Sulphate	mg/L	500	a	715 - 3180	148 - 2220	1261	1261	
Ammonia	mg/L			3 - 31	0 - 28	6.00		
TKN	mg/L			51 - 110	0.19 - 36.4	6.80		
Nitrate	mg/L	10	h	0	0 - 3.7	0.33	2.74	
Nitrite	mg/L	1	h	0.01 - 0.029	0 - 3.32	0.18	0.39	
Phosphate	mg/L			0 - 1.7	0 - 0.1	0.01		
Aluminum	mg/L	0.1	o	0 - 0.58	0 - 0.57	0.06	0.08	
Barium	mg/L	1	h	0.05 - 2.07	0 - 0.05	0.02	0.27	
Beryllium	mg/L			0 - 0.001	0 - 0	0.00		
Boron	mg/L	5	h	0 - 0.627	0.278 - 12	2.77	3.33	
Cadmium	mg/L	0.005	h	0 - 0.001	0 - 0.007	0.001	0.002	
Chromium	mg/L	0.05	h	0 - 0.02	0	0	0.013	
Cobalt	mg/L			0 - 0.15	0	0		
Copper	mg/L	1	a	0 - 0.15	0 - 0.1	0.004	0.502	
Lead	mg/L	0.01	h	0 - 0.04	0	0	0.003	
Iron	mg/L	0.3	a	0 - 0.63	0 - 0.87	0.14	0.221	
Manganese	mg/L	0.05	a	0 - 0.44	0 - 0.25	0.08	0.083	
Molybdenum	mg/L			0 - 1.1	0	0		
Nickel	mg/L			0 - 0.78	0	0		
Silica	mg/L			7.17 - 37.3	2.69 - 5.86	4.10		
Silver	mg/L			0	0 - 0.005	0.0002		
Strontium	mg/L			2.41 - 10.9	0.97 - 9.37	4.96		
Titanium	mg/L			0 - 0.011	0 - 0.01	0.003		
Vanadium	mg/L			0 - 0.07	0 - 0.012	0.001		
Zinc	mg/L	5	a	0 - 0.9	0 - 0.2	0.03	2.52	
Thorium	mg/L							
Zircon	mg/L							
Phenols	µg/L			180 - 47500	0 - 4.5	0.30		

h - health related objective

a - aesthetic objective associated with taste, smell and colour

o - operational objective to ensure efficient treatment of water

TABLE D1: Assessment of Critical Contaminants

Mid Flow Zone

Compound		ODWO		Predicted East Quarry Landfill Leachate	Background Range in Mid Flow Zone		Reasonable Use
units					Range	Average	
					Total # Samples 57		Based on average
pH	pH units	6.5-8.5	o	7.4 - 12.83	6.91 - 8.13	7.42	MFZ
Conductivity	µmhos/cm			814 - 12750	1172 - 84000	13688	
TDS	mg/L	500	a	598 - 14256	884 - 84224	12896	12896
COD	mg/L			800 - 5000	0 - 1700	163	
TOC	mg/L			154 - 1310	0 - 263	17.08	
Alkalinity	mg CaCO ₃ /L	30-500	o	232 - 4550	123 - 370	214	357
Hardness	mg CaCO ₃ /L	80-100	o	109 - 2552	673 - 29270	4854	4854
Calcium	mg/L			343 - 1820	145 - 8090	1364	
Magnesium	mg/L			0 - 26.4	46.1 - 2190	350	
Sodium	mg/L	200	a	161 - 739	14.3 - 12600	1782	1782
Potassium	mg/L			1550 - 2360	0 - 226	45	
Chloride	mg/L	250	a	34 - 161	42.7 - 50400	5798	5798
Fluoride	mg/L	1.5	h	0 - 3.9	0.2 - 1	0.54	0.78
Bromide	mg/L			0 - 78	0 - 575	62	
Sulphate	mg/L	500	a	715 - 3180	302 - 2130	1309	1309
Ammonia	mg/L			3 - 31	0 - 25	5.27	
TKN	mg/L			51 - 110	0.21 - 31	5.92	
Nitrate	mg/L	10	h	0	0 - 1.5	0.05	2.54
Nitrite	mg/L	1	h	0.01 - 0.029	0 - 0.061	0.007	0.26
Phosphate	mg/L			0 - 1.7	0 - 1	0.06	
Aluminum	mg/L	0.1	o	0 - 0.58	0 - 0.39	0.06	0.08
Barium	mg/L	1	h	0.05 - 2.07	0 - 0.083	0.033	0.28
Beryllium	mg/L			0 - 0.001	0 - 0.001	0.00001	
Boron	mg/L	5	h	0 - 0.627	0.1 - 30.1	2.43	3.07
Cadmium	mg/L	0.005	h	0 - 0.001	0 - 0.008	0.001	0.002
Chromium	mg/L	0.05	h	0 - 0.02	0	0	0.013
Cobalt	mg/L			0 - 0.15	0	0	
Copper	mg/L	1	a	0 - 0.15	0 - 0.29	0.01	0.504
Lead	mg/L	0.01	h	0 - 0.04	0	0	0.003
Iron	mg/L	0.3	a	0 - 0.63	0 - 0.92	0.10	0.199
Manganese	mg/L	0.05	a	0 - 0.44	0 - 0.8	0.16	0.160
Molybdenum	mg/L			0 - 1.1	0	0	
Nickel	mg/L			0 - 0.78	0	0	
Silica	mg/L			7.17 - 37.3	2.23 - 6.58	3.94	
Silver	mg/L			0	0 - 0.007	0.0001	
Strontium	mg/L			2.41 - 10.9	1.39 - 160	22.7	
Titanium	mg/L			0 - 0.011	0 - 0.1	0.01	
Vanadium	mg/L			0 - 0.07	0 - 0.016	0.001	
Zinc	mg/L	5	a	0 - 0.9	0 - 0.2	0.01	2.51
Thorium	mg/L						
Zircon	mg/L						
Phenols	µg/L			180 - 47500	0 - 8	0.26	

h - health related objective
a - aesthetic objective associated with taste, smell and colour
o - operational objective to ensure efficient treatment of water

TABLE D1: Assessment of Critical Contaminants

Lower Flow Zone

Compound		ODWO		Predicted East Quarry Landfill Leachate		Background Range in Lower Flow Zone		Reasonable Use
units						Range	Average	
						Total # Samples 48		Based on average
pH	pH units	6.5-8.5	o	7.4 - 12.83	6.75 - 8.22	7.38	LFZ	
Conductivity	µmhos/cm			814 - 12750	1680 - 96200	24635		
TDS	mg/L	500	a	598 - 14256	1188 - 1E+05	24634	24634	
COD	mg/L			800 - 5000	6 - 1460	254		
TOC	mg/L			154 - 1310	0 - 532	57		
Alkalinity	mg CaCO ₃ /L	30-500	o	232 - 4550	72.9 - 305	200	350	
Hardness	mg CaCO ₃ /L	80-100	o	109 - 2552	705.7 - 48390	9157	9157	
Calcium	mg/L			343 - 1820	181 - 13200	2472		
Magnesium	mg/L			0 - 26.4	61.3 - 3710	718		
Sodium	mg/L	200	a	161 - 739	48.3 - 19100	3618	3618	
Potassium	mg/L			1550 - 2360	0 - 460	74		
Chloride	mg/L	250	a	34 - 161	159 - 60100	12278	12278	
Fluoride	mg/L	1.5	h	0 - 3.9	0 - 1	0.28	0.58	
Bromide	mg/L			0 - 78	0 - 771	132		
Sulphate	mg/L	500	a	715 - 3180	134 - 1960	917	917	
Ammonia	mg/L			3 - 31	0.1 - 34	7.26		
TKN	mg/L			51 - 110	0.17 - 34	7.23		
Nitrate	mg/L	10	h	0	0 - 1	0.11	2.58	
Nitrite	mg/L	1	h	0.01 - 0.029	0 - 3.41	0.12	0.34	
Phosphate	mg/L			0 - 1.7	0 - 1	0.17		
Aluminum	mg/L	0.1	o	0 - 0.58	0 - 0.31	0.03	0.07	
Barium	mg/L	1	h	0.05 - 2.07	0 - 0.28	0.09	0.32	
Beryllium	mg/L			0 - 0.001	0 - 0.001	0.00004		
Boron	mg/L	5	h	0 - 0.627	0 - 86.4	9.59	9.59	
Cadmium	mg/L	0.005	h	0 - 0.001	0 - 0.467	0.020	0.020	
Chromium	mg/L	0.05	h	0 - 0.02	0 - 0.05	0.002	0.014	
Cobalt	mg/L			0 - 0.15	0 - 0.1	0.002		
Copper	mg/L	1	a	0 - 0.15	0 - 0.26	0.016	0.508	
Lead	mg/L	0.01	h	0 - 0.04	0 - 0.03	0.001	0.003	
Iron	mg/L	0.3	a	0 - 0.63	0 - 2.5	0.16	0.229	
Manganese	mg/L	0.05	a	0 - 0.44	0 - 2.5	0.39	0.389	
Molybdenum	mg/L			0 - 1.1	0 - 0.3	0.01		
Nickel	mg/L			0 - 0.78	0 - 0.08	0.003		
Silica	mg/L			7.17 - 37.3	1.68 - 14.1	4.31		
Silver	mg/L			0	0 - 0.5	0.02		
Strontium	mg/L			2.41 - 10.9	2.95 - 262	51.78		
Titanium	mg/L			0 - 0.011	0 - 0.15	0.03		
Vanadium	mg/L			0 - 0.07	0 - 0.025	0.002		
Zinc	mg/L	5	a	0 - 0.9	0 - 0.2	0.04	2.52	
Thorium	mg/L				0	0		
Zircon	mg/L				0 - 0.03	0.01		
Phenols	µg/L			180 - 47500	0 - 14.5	0.41		

h - health related objective
a - aesthetic objective associated with taste, smell and colour
o - operational objective to ensure efficient treatment of water

TABLE D1: Assessment of Critical Contaminants

Rochester Shale

Compound		ODWO		Predicted East Quarry Landfill Leachate	Background Range in Rochester Shale		Reasonable Use
units					Range	Average	
					Total # Samples 6		Based on average
pH	pH units	6.5-8.5	o	7.4 - 12.83	7.04 - 8.3	7.60	Rochester
Conductivity	µmhos/cm			814 - 12750	15800 - 57100	41750	
TDS	mg/L	500	a	598 - 14256	11926 - 58440	40107	40107
COD	mg/L			800 - 5000	0 - 750	441	
TOC	mg/L			154 - 1310	0 - 96	44	
Alkalinity	mg CaCO ₃ /L	30-500	o	232 - 4550	103 - 208	150	325
Hardness	mg CaCO ₃ /L	80-100	o	109 - 2552	3634 - 17830	12135	12135
Calcium	mg/L			343 - 1820	1030 - 5020	3378	
Magnesium	mg/L			0 - 26.4	251 - 1280	892	
Sodium	mg/L	200	a	161 - 739	2120 - 9240	6565	6565
Potassium	mg/L			1550 - 2360	63 - 319	201	
Chloride	mg/L	250	a	34 - 161	5370 - 30400	20695	20695
Fluoride	mg/L	1.5	h	0 - 3.9	0.1 - 0.6	0.3	0.60
Bromide	mg/L			0 - 78	52.6 - 302	225	
Sulphate	mg/L	500	a	715 - 3180	1160 - 1480	1277	1277
Ammonia	mg/L			3 - 31	5.7 - 23	17	
TKN	mg/L			51 - 110	6.5 - 25	19	
Nitrate	mg/L	10	h	0	0 - 0.4	0.07	2.55
Nitrite	mg/L	1	h	0.01 - 0.029	0.004 - 0.14	0.065	0.30
Phosphate	mg/L			0 - 1.7	0 - 1	0.25	
Aluminum	mg/L	0.1	o	0 - 0.58	0 - 0.3	0.07	0.09
Barium	mg/L	1	h	0.05 - 2.07	0.098 - 0.204	0.158	0.37
Beryllium	mg/L			0 - 0.001	0	0	
Boron	mg/L	5	h	0 - 0.627	2.07 - 104	55.41	55.41
Cadmium	mg/L	0.005	h	0 - 0.001	0 - 0.006	0.001	0.002
Chromium	mg/L	0.05	h	0 - 0.02	0	0	0.013
Cobalt	mg/L			0 - 0.15	0	0	
Copper	mg/L	1	a	0 - 0.15	0 - 0.1	0.02	0.508
Lead	mg/L	0.01	h	0 - 0.04	0	0	0.003
Iron	mg/L	0.3	a	0 - 0.63	0 - 0.06	0.01	0.155
Manganese	mg/L	0.05	a	0 - 0.44	0.1 - 0.7	0.41	0.410
Molybdenum	mg/L			0 - 1.1	0	0	
Nickel	mg/L			0 - 0.78	0	0	
Silica	mg/L			7.17 - 37.3	2.77 - 5.3	3.7	
Silver	mg/L			0	0	0	
Strontium	mg/L			2.41 - 10.9	14.3 - 98.6	66.1	
Titanium	mg/L			0 - 0.011	0 - 0.06	0.03	
Vanadium	mg/L			0 - 0.07	0 - 0.008	0.003	
Zinc	mg/L	5	a	0 - 0.9	0 - 0.2	0.035	2.52
Thorium	mg/L						
Zircon	mg/L						
Phenols	µg/L			180 - 47500	0 - 3	0.98	

h - health related objective
a - aesthetic objective associated with taste, smell and colour
o - operational objective to ensure efficient treatment of water

Table D2: Assessment of Critical Organic Contaminants

all concentrations in µg/L

Compound	ODWO			8-1			28-11			30-1		
	Limit	Type	RUP	max	min	avg	max	min	avg	max	min	avg
MISA Group 20 – Acid Extractables												
2,3,4,5-TETRACHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,3,4,6-TETRACHLOROPHENOL	100	H	25	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,3,5,6-TETRACHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,3,4-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,3,5-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4,5-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4,6-TRICHLOROPHENOL	5	H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DIMETHYLPHENOL				ND	ND	ND	6	ND	0.8571	646	42.4	258.64
2,4-DINITROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DICHLOROPHENOL	900	H	225	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,6-DICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
4,6-DINITRO-O-CRESOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2-CHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
4-CHLORO-3-METHYLPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
4-NITROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
M-CRESOL & P-CRESOL				ND	ND	ND	21.2	ND	3.5333	1310	16.6	426.09
O-CRESOL				ND	ND	ND	2.9	ND	0.4833	67.8	4.3	25.843
PENTACHLOROPHENOL	60	A	30	ND	ND	ND	ND	ND	ND	ND	ND	ND
PHENOL				ND	ND	ND	176	ND	43.714	2330	184	1080.6
NITROPHENOL							ND	ND		20	ND	10
2-METHYL-4-6-DINITROPHENOL							ND	ND		21	ND	10.5
Misa Group 19 – Base/Neutral Extractables												
ACENAPHTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
5-NITROACENAPHTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ACENAPHTHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ANTHRACENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZ(A)ANTHRACENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZO(A)PYRENE	0.01	H	0.0025	ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZO(B)FLUORANTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZO(G,H,I)PERYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZO(K)FLUORANTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIPHENYL				ND	ND	ND	ND	ND	ND	ND	ND	ND
CAMPHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1-CHLORONAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
2-CHLORONAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHRYSENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIBENZ(A,H)ANTHRACENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
FLUORANTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
FLUORENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
INDENO(1,2,3-CD)PYRENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
INDOLE				ND	ND	ND	ND	ND	ND	54.3	ND	20.057
1-METHYLNAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
2-METHYLNAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
NAPHTHALENE				ND	ND	ND	ND	ND	ND	122	ND	19.225
PERYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
PHENANTHRENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
PYRENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZYL BUTYL PHTHALATE				ND	ND	ND	ND	ND	ND	0.6	ND	0.075
BIS(2-ETHYLHEXYL)PHTHALATE				6	ND	1	10.4	ND	1.4857	36.4	ND	4.55
DI-N-BUTYL PHTHALATE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DI-N-OCTYL PHTHALATE				ND	ND	ND	ND	ND	ND	ND	ND	ND
4-BROMOPHENYL PHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
4-CHLOROPHENYL PHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIS(2-CHLOROISOPROPYL)ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIS(2-CHLOROETHYL)ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIPHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DINITROTOLUENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,6-DINITROTOLUENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIS(2-CHLOROETHOXY)METHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIPHENYLAMINE & N-NITROSODIPHA				ND	ND	ND	ND	ND	ND	ND	ND	ND
N-NITROSODI-N-PROPYLAMINE				ND	ND	ND	ND	ND	ND	ND	ND	ND

ODWO Ontario Drinking Water Objective
 (H – Health, A – Aesthetic, inter H – interim health)
 RUP – Reasonable Use Policy Guideline
 Calculated assuming background concentration equal to 0 µg/L

Table D2: Assessment of Critical Organic Contaminants

Compound	all concentrations in µg/L											
	ODWO			8-1			28-11			30-1		
	Limit	Type	RUP	max	min	avg	max	min	avg	max	min	avg
MISA Group 22 – Organochlorine Compounds												
ALDRIN				ND	ND	ND	0.003	ND	0.0004	0.001	ND	0.0002
DIELDRIN				ND	ND	ND	0.0006	ND	9E-05	ND	ND	ND
ALDRIN + DIELDRIN	0.7	H	0.175	0			0.0036			0.001		
ALPHA-BHC				ND	ND	ND	0.0008	ND	0.0001	0.0015	ND	0.0004
BETA-BHC				ND	ND	ND	ND	ND	ND	0.0043	ND	0.0012
DELTA-BHC				ND	ND	ND	ND	ND	ND	0.005	ND	0.0006
GAMMA-BHC				ND	ND	ND	ND	ND	ND	0.0008	ND	0.0001
CHLORDANE	7	H	1.75	ND	ND	ND	ND	ND	ND	ND	ND	ND
DDD				ND	ND	ND	ND	ND	ND	0.001	ND	0.0001
DDE				0.001	ND	0.0002	ND	ND	ND	ND	ND	ND
DDT	30	H	7.5	ND	ND	ND	ND	ND	ND	0.001	ND	0.0001
2,4-DDT				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDOSULFAN I				ND	ND	ND	ND	ND	ND	0.001	ND	0.0001
ENDOSULFAN II				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDOSULFAN SULPHATE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDRIN				ND	ND	ND	0.003	ND	0.0004	0.003	ND	0.0004
ENDRIN ALDEHYDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
HEPTACHLOR				0.0023	ND	0.0006	0.002	ND	0.0004	0.003	ND	0.0005
HEPTACHLOR EPOXIDE				0.001	ND	0.0002	0.001	ND	0.0001	0.006	ND	0.001
HEPTACHLOR + HEPTACHLOR EPOXIDE	3	inter H	0.75	0.0033			0.003			0.009		
METHOXYCHLOR	900	H	225	ND	ND	ND	ND	ND	ND	ND	ND	ND
MIREX				ND	ND	ND	ND	ND	ND	ND	ND	ND
TOXAPHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
PCB's	3	H	0.75	ND	ND	ND	ND	ND	ND	0.3242	ND	0.0405
MISA Group 17												
BENZENE	5	H	1.25	ND	ND	ND	0.1	ND	0.0143	3.5	0.5	1.6125
ETHYLBENZENE	2.4	A	1.2	0.2	ND	0.033	0.3	ND	0.0714	0.8	ND	0.2
STYRENE				ND	ND	ND	ND	ND	ND	0	ND	0
TOLUENE	24	A	12	ND	ND	ND	151	ND	21.571	2	ND	0.475
O-XYLENE	300	A	150	ND	ND	ND	0.3	ND	0.0714	2.3	ND	0.375
M-XYLENE + P-XYLENE	300	A	150	ND	ND	ND	0.4	ND	0.1	2.4	ND	0.4
MISA Group 18												
ACROLEIN				ND	ND	ND	ND	ND	ND	ND	ND	ND
ACRYLONITRILE				ND	ND	ND	ND	ND	ND	ND	ND	ND
MISA Group 16 – Halogenated VOC's												
1,1,2,2-TETRACHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,2-TRICHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1-DICHLOROETHANE				ND	ND	ND	ND	ND	ND	0.4	ND	0.1375
1,1-DICHLOROETHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DICHLOROBENZENE	200	H	50	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DICHLOROETHANE	5	inter H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DICHLOROPROPANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3-DICHLOROBENZENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,4-DICHLOROBENZENE	5	H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
BROMOFORM				ND	ND	ND	ND	ND	ND	ND	ND	ND
BROMOMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CARBON TETRACHLORIDE	5	H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROBENZENE				ND	ND	ND	ND	ND	ND	0.7	ND	0.0875
CHLOROFORM				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CIS-1,3-DICHLOROPROPYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIBROMOCHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ETHYLENE DIBROMIDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
METHYLENE CHLORIDE				330	ND	96	12.7	ND	2.1167	81.5	ND	11.643
TETRACHLOROETHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
TRANS-1,2-DICHLOROETHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
TRANS-1,3-DICHLOROPROPYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
TRICHLOROETHYLENE	50	H	12.5	ND	ND	ND	ND	ND	ND	0.3	ND	0.0375
TRICHLOROFLUOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
VINYL CHLORIDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,1-TRICHLOROETHANE							ND	ND	ND	0.4	ND	0.2
DICHLOROMETHANE	50	H	12.5				ND	ND	ND	ND	ND	ND
CIS-1,2-DICHLOROETHENE							ND	ND	ND	ND	ND	ND
BROMODICHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROETHANE							ND	ND	ND	ND	ND	ND
1,2-DIBROMOETHANE							ND	ND	ND	ND	ND	ND

ODWO Ontario Drinking Water Objective
 (H - Health, A - Aesthetic, inter H - interim health)
 RUP - Reasonable Use Policy Guideline
 Calculated assuming background concentration equal to 0 µg/L

Table D2: Assessment of Critical Organic Contaminants

all concentrations in µg/L

Compound	ODWO			30-II			31-II			32-II			
	Limit	Type	RUP	max	min	avg	max	min	avg	max	min	avg	
MISA Group 20 - Acid Extractables													
2,3,4,5-TETRACHLOROPHENOL				5.3	ND	1.0143		2.9	ND	0.4143	ND	ND	ND
2,3,4,6-TETRACHLOROPHENOL	100	H	25	3.7	ND	1.0429	ND	ND	ND	ND	ND	ND	
2,3,5,6-TETRACHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2,3,4-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2,3,5-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2,4,5-TRICHLOROPHENOL				7.1	0	1.2143	ND	ND	ND	ND	ND	ND	
2,4,6-TRICHLOROPHENOL	5	H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND	
2,4-DIMETHYLPHENOL				584	79.5	253.19	231	2.3	125.21	4680	51.5	1360	
2,4-DINITROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2,4-DICHLOROPHENOL	900	H	225	8.9	ND	1.1125	ND	ND	ND	ND	ND	ND	
2,6-DICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
4,6-DINITRO-O-CRESOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2-CHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
4-CHLORO-3-METHYLPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
4-NITROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
M-CRESOL & P-CRESOL				1040	104	313.43	1310	ND	235.21	8540	667	4715.3	
O-CRESOL				56.2	18.2	41.614	66.1	ND	27.129	245	39.5	166.93	
PENTACHLOROPHENOL	60	A	30	ND	ND	ND	3	ND	0.375	ND	ND	ND	
PHENOL				1590	ND	761.75	1800	ND	262.04	13500	662	5830.3	
NITROPHENOL				ND	ND	ND	20	ND	10	ND	ND	ND	
2-METHYL-4-6-DINITROPHENOL				ND	ND	ND	21	ND	10.5	ND	ND	ND	
Misa Group 19 - Base/Neutral Extractables													
ACENAPHTHENE				1.1	ND	0.1375	ND	ND	ND	4.8	ND	1.15	
5-NITROACENAPHTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
ACENAPHTHYLENE				1.8	ND	0.225	ND	ND	ND	4	ND	0.925	
ANTHRACENE				0	ND	0	ND	ND	ND	2.1	ND	0.4375	
BENZ(A)ANTHRACENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
BENZO(A)PYRENE	0.01	H	0.0025	ND	ND	ND	ND	ND	ND	ND	ND	ND	
BENZO(B)FLUORANTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
BENZO(G,H,I)PERYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
BENZO(K)FLUORANTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
BIPHENYL				ND	ND	ND	ND	ND	ND	ND	ND	ND	
CAMPHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
1-CHLORONAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2-CHLORONAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
CHRYSENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
DIBENZ(A,H)ANTHRACENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
FLUORANTHENE				1.2	ND	0.225	ND	ND	ND	4.1	ND	0.6	
FLUORENE				2.9	ND	0.65	ND	ND	ND	2.3	ND	0.5875	
INDENO(1,2,3-CD)PYRENE				0	ND	0	ND	ND	ND	ND	ND	ND	
INDOLE				38.3	ND	19.2	42.3	ND	6.0429	162	20.5	58.914	
1-METHYL NAPHTHALENE				3.9	ND	1.0714	ND	ND	ND	0	ND	0	
2-METHYL NAPHTHALENE				17.5	ND	4.5286	ND	ND	ND	2.5	ND	0.6143	
NAPHTHALENE				306	0.5	91.875	18.6	ND	2.4875	120	49.9	81.588	
PERYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
PHENANTHRENE				5.3	ND	1.6125	0.2	ND	0.025	9.2	ND	1.675	
PYRENE				0.9	ND	0.1875	ND	ND	ND	3.8	ND	0.5375	
BENZYL BUTYL PHTHALATE				0.6	ND	0.075	ND	ND	ND	ND	ND	ND	
BIS(2-ETHYLHEXYL)PHTHALATE				26.2	ND	3.4875	10.7	ND	1.3375	2.2	ND	0.275	
DI-N-BUTYL PHTHALATE				ND	ND	ND	25.5	ND	3.1875	ND	ND	ND	
DI-N-OCTYL PHTHALATE				ND	ND	ND	6.6	ND	1.65	ND	ND	ND	
4-BROMOPHENYL PHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND	
4-CHLOROPHENYL PHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND	
BIS(2-CHLOROISOPROPYL)ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND	
BIS(2-CHLOROETHYL)ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND	
DIPHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2,4-DINITROTOLUENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
2,6-DINITROTOLUENE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
BIS(2-CHLOROETHOXY)METHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND	
DIPHENYLAMINE & N-NITROSODIPHA				10.3	ND	1.4714	ND	ND	ND	17.9	ND	4.9714	
N-NITROSODI-N-PROPYLAMINE				ND	ND	ND	ND	ND	ND	ND	ND	ND	

ODWO Ontario Drinking Water Objective

(H - Health, A - Aesthetic, Inter H - Interim health)

RUP - Reasonable Use Policy Guideline

Calculated assuming background concentration equal to 0 µg/L

Table D2: Assessment of Critical Organic Contaminants

Compound	all concentrations in µg/L											
	ODWO			30-II			31-II			32-II		
	Limit	Type	RUP	max	min	avg	max	min	avg	max	min	avg
MISA Group 22 – Organochlorine Compounds												
ALDRIN				ND	ND	ND	0.002	ND	0.0004	0.004	ND	0.0006
DIELDRIN				0.019	ND	0.0052	0.0018	ND	0.0003	ND	ND	ND
ALDRIN + DIELDRIN	0.7	H	0.175	0.019			0.0038			0.004		
ALPHA-BHC				0.0026	ND	0.0004	ND	ND	ND	0.012	ND	0.004
BETA-BHC				0.034	0.0046	0.0228	0.0022	ND	0.0006	ND	ND	ND
DELTA-BHC				0.0025	ND	0.0003	0.0021	ND	0.0003	ND	ND	ND
GAMMA-BHC				0.002	ND	0.0003	0.002	ND	0.0005	0.004	ND	0.0005
CHLORDANE	7	H	1.75	ND	ND	ND	ND	ND	ND	ND	ND	ND
DDD				0.0035	ND	0.0007	ND	ND	ND	0.01	ND	0.0013
DDE				0.0021	ND	0.0005	ND	ND	ND	0.007	ND	0.0009
DDT	30	H	7.5	0.003	ND	0.0004	ND	ND	ND	ND	ND	ND
2,4-DDT				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDOSULFAN I				0.0027	ND	0.0003	ND	ND	ND	0.004	ND	0.0005
ENDOSULFAN II				ND	ND	ND	0.006	ND	0.0008	0.052	ND	0.0065
ENDOSULFAN SULPHATE				ND	ND	ND	ND	ND	ND	0.076	ND	0.0095
ENDRIN				0.003	ND	0.0005	0.002	ND	0.0003	0.0047	ND	0.0006
ENDRIN ALDEHYDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
HEPTACHLOR				0.0026	ND	0.0006	0.004	ND	0.0011	0.0159	ND	0.0039
HEPTACHLOR EPOXIDE				0.02	ND	0.0026	0.001	ND	0.0002	0.0365	ND	0.0072
HEPTACHLOR + HEPTACHLOR EPOXIDE	3	inter H	0.75	0.0226			0.005			0.0524		
METHOXYCHLOR	900	H	225	ND	ND	ND	ND	ND	ND	0.024	ND	0.003
MIREX				ND	ND	ND	ND	ND	ND	ND	ND	ND
TOXAPHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
PCB's	3	H	0.75	ND	ND	ND	0.3178	ND	0.0397	ND	ND	ND
MISA Group 17												
BENZENE	5	H	1.25	13	3.1	6.8875	1	ND	0.5625	2.2	ND	1.525
ETHYLBENZENE	2.4	A	1.2	1.1	ND	0.5625	0.3	ND	0.0625	6.2	ND	2.5375
STYRENE				ND	ND	ND	0	ND	0	1.1	ND	0.3875
TOLUENE	24	A	12	6.2	2.7	4.4375	0.9	ND	0.425	10.6	ND	3.25
O-XYLENE	300	A	150	4.6	1.3	2.475	0.8	ND	0.225	1.8	ND	1.15
M-XYLENE + P-XYLENE	300	A	150	4.8	1.7	3	0.8	ND	0.225	2.5	ND	1.4
MISA Group 18												
ACROLEIN				ND	ND	ND	ND	ND	ND	ND	ND	ND
ACRYLONITRILE				ND	ND	ND	ND	ND	ND	ND	ND	ND
MISA Group 16 – Halogenated VOC's												
1,1,2-TETRACHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,2-TRICHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1-DICHLOROETHANE				1.5	ND	1.125	0.5	ND	0.15	0.5	ND	0.2875
1,1-DICHLOROETHYLENE				ND	ND	ND	0	ND	0	ND	ND	ND
1,2-DICHLOROBENZENE	200	H	50	0.4	ND	0.075	ND	ND	ND	0.2	ND	0.075
1,2-DICHLOROETHANE	5	inter H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DICHLOROPROPANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3-DICHLOROBENZENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,4-DICHLOROBENZENE	5	H	1.25	0.3	ND	0.0625	0.1	ND	0.0125	49.6	ND	12.275
BROMOFORM				ND	ND	ND	ND	ND	ND	ND	ND	ND
BROMOMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CARBON TETRACHLORIDE	5	H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROBENZENE				1.1	ND	0.3125	ND	ND	ND	ND	ND	ND
CHLOROFORM				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CIS-1,3-DICHLOROPROPYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIBROMOCHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ETHYLENE DIBROMIDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
METHYLENE CHLORIDE				42.5	ND	6.0714	61.2	ND	8.7429	380	ND	54.286
TETRACHLOROETHYLENE				0.6	ND	0.075	ND	ND	ND	ND	ND	ND
TRANS-1,2-DICHLOROETHYLENE				0.2	ND	0.025	0.1	ND	0.0125	ND	ND	ND
TRANS-1,3-DICHLOROPROPYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
TRICHLOROETHYLENE	50	H	12.5	1.7	ND	0.7375	1.4	ND	0.375	0.4	ND	0.175
TRICHLOROFLUOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
VINYL CHLORIDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,1-TRICHLOROETHANE				0.4	ND	0.4	ND	ND	ND	ND	ND	ND
DICHLOROMETHANE	50	H	12.5	ND	ND	ND	ND	ND	ND	ND	ND	ND
CIS-1,2-DICHLOROETHENE				0.6	ND	0.6	0.2	ND	0.2	0.2	ND	0.2
BROMODICHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DIBROMOETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND

ODWO - Ontario Drinking Water Objective
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 RUP - Reasonable Use Policy Guideline
 Calculated assuming background concentration equal to 0 µg/L

Table D2: Assessment of Critical Organic Contaminants

all concentrations in µg/L

Compound	ODWO			33-II			38-I			44-I		
	Limit	Type	RUP	max	min	avg	max	min	avg	max	min	avg
MISA Group 20 – Acid Extractables												
2,3,4,5-TETRACHLOROPHENOL				ND	ND	ND	ND	ND	ND			
2,3,4,6-TETRACHLOROPHENOL	100	H	25	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,3,5,6-TETRACHLOROPHENOL				ND	ND	ND	ND	ND	ND			
2,3,4-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,3,5-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4,5-TRICHLOROPHENOL				ND	ND	ND	ND	ND	ND			
2,4,6-TRICHLOROPHENOL	5	H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DIMETHYLPHENOL				147	ND	28.05	1.8	ND	0.225	ND	ND	ND
2,4-DINITROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DICHLOROPHENOL	900	H	225	1.5	ND	0.1875	ND	ND	ND	ND	ND	ND
2,6-DICHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
4,6-DINITRO-O-CRESOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
2-CHLOROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
4-CHLORO-3-METHYLPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
4-NITROPHENOL				ND	ND	ND	ND	ND	ND	ND	ND	ND
M-CRESOL & P-CRESOL				1280	ND	193.07	0.5	ND	0	ND	ND	ND
O-CRESOL				61.9	ND	10.814	6.8	ND	0.97	ND	ND	ND
PENTACHLOROPHENOL	60	A	30	ND	ND	ND	ND	ND	ND	ND	ND	ND
PHENOL				1780	ND	557.16	25.5	ND	8.5	ND	ND	ND
NITROPHENOL				20	ND	10	40.3	ND	13.43			
2-METHYL-4,6-DINITROPHENOL				21	ND	10.5	ND	ND	ND			
Misa Group 19 – Base/Neutral Extractables												
ACENAPHTHENE				0.5	ND	0.0625	ND	ND	ND	ND	ND	ND
5-NITROACENAPHTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ACENAPHTHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ANTHRACENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZ(A)ANTHRACENE				0.8	ND	0.1	ND	ND	ND	ND	ND	ND
BENZO(A)PYRENE	0.01	H	0.0025	ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZO(B)FLUORANTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZO(G,H,I)PERYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZO(K)FLUORANTHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIPHENYL				ND	ND	ND	ND	ND	ND	ND	ND	ND
CAMPHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1-CHLORONAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
2-CHLORONAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHRYSENE				0.9	ND	0.1125	ND	ND	ND	ND	ND	ND
DIBENZ(A,H)ANTHRACENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
FLUORANTHENE				0.8	ND	0.1	ND	ND	ND	ND	ND	ND
FLUORENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
INDENO(1,2,3-CD)PYRENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
INDOLE				21.4	ND	3.4	ND	ND	ND	ND	ND	ND
1-METHYL NAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
2-METHYL NAPHTHALENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
NAPHTHALENE				16.3	0	4.1	ND	ND	ND	ND	ND	ND
PERYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
PHENANTHRENE				0.8	0	0.175	ND	ND	ND	ND	ND	ND
PYRENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BENZYL BUTYL PHTHALATE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIS(2-ETHYLHEXYL)PHTHALATE				2.4	0	0.5625	4.6	ND	0.9875	ND	ND	ND
DI-N-BUTYL PHTHALATE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DI-N-OCTYL PHTHALATE				ND	ND	ND	2	ND	0.5	ND	ND	ND
4-BROMOPHENYL PHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
4-CHLOROPHENYL PHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIS(2-CHLOROISOPROPYL)ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIS(2-CHLOROETHYL)ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIPHENYL ETHER				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DINITROTOLUENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
2,6-DINITROTOLUENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BIS(2-CHLOROETHOXY)METHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIPHENYLAMINE & N-NITROSODIPHA				ND	ND	ND	ND	ND	ND	ND	ND	ND
N-NITROSODI-N-PROPYLAMINE				ND	ND	ND	ND	ND	ND	ND	ND	ND

ODWO Ontario Drinking Water Objective
 (H – Health, A – Aesthetic, inter H – interim health)
 RUP – Reasonable Use Policy Guideline
 Calculated assuming background concentration equal to 0 µg/L

Table D2: Assessment of Critical Organic Contaminants

Compound	all concentrations in µg/L											
	ODWO			33-II			36-I			44-I		
	Limit	Type	RUP	max	min	avg	max	min	avg	max	min	avg
MISA Group 22 – Organochlorine Compounds												
ALDRIN				0.002	ND	0.0007	ND	ND	ND	ND	ND	ND
DIELDRIN				0.0415	ND	0.0145	0.0005	ND	6E-05	ND	ND	ND
ALDRIN + DIELDRIN	0.7	H	0.175	0.0435			0.0005			0		
ALPHA-BHC				0.015	ND	0.0049	ND	ND	ND	ND	ND	ND
BETA-BHC				0.027	ND	0.0131	ND	ND	ND	ND	ND	ND
DELTA-BHC				ND	ND	ND	ND	ND	ND	ND	ND	ND
GAMMA-BHC				0.0005	ND	0.0001	0.0025	ND	0	ND	ND	ND
CHLORDANE	7	H	1.75	ND	ND	ND	ND	ND	ND	ND	ND	ND
DDD				0.004	ND	0.0009	ND	ND	ND	ND	ND	ND
DDE				0.0026	ND	0.0006	ND	ND	ND	ND	ND	ND
DDT	30	H	7.5	ND	ND	ND	ND	ND	ND	ND	ND	ND
2,4-DDT				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDOSULFAN I				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDOSULFAN II				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDOSULFAN SULPHATE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ENDRIN				0.0047	ND	0.0012	ND	ND	ND	ND	ND	ND
ENDRIN ALDEHYDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
HEPTACHLOR				0.003	ND	0.0008	0.087	ND	0.011	ND	ND	ND
HEPTACHLOR EPOXIDE				0.0008	ND	0.0001	ND	ND	ND	ND	ND	ND
HEPTACHLOR + HEPTACHLOR EPOXIDE	3	inter H	0.75	0.0038			0.087			0		
METHOXYCHLOR	900	H	225	ND	ND	ND	ND	ND	ND	ND	ND	ND
MIREX				ND	ND	ND	ND	ND	ND	ND	ND	ND
TOXAPHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
PCB's	3	H	0.75	ND	ND	ND	4.09	ND	0.5113	ND	ND	ND
MISA Group 17												
BENZENE	5	H	1.25	1.8	ND	0.8375	ND	ND	ND	ND	ND	ND
ETHYLBENZENE	2.4	A	1.2	0.1	ND	0.0125	ND	ND	ND	ND	ND	ND
STYRENE				0	ND	0	ND	ND	ND	ND	ND	ND
TOLUENE	24	A	12	1.8	ND	0.825	0.2	ND	0.025	0.2	ND	0.1
O-XYLENE	300	A	150	0.9	ND	0.1625	ND	ND	ND	ND	ND	ND
M-XYLENE + P-XYLENE	300	A	150	1.1	ND	0.2375	0.2	ND	0.025	0.1	ND	0.05
MISA Group 18												
ACROLEIN				ND	ND	ND	ND	ND	ND	ND	ND	ND
ACRYLONITRILE				ND	ND	ND	ND	ND	ND	ND	ND	ND
MISA Group 16 – Halogenated VOC's												
1,1,2,2-TETRACHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,2-TRICHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1-DICHLOROETHANE				0.1	ND	0.0125	ND	ND	ND	ND	ND	ND
1,1-DICHLOROETHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DICHLOROBENZENE	200	H	50	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DICHLOROETHANE	5	inter H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DICHLOROPROPANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,3-DICHLOROBENZENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,4-DICHLOROBENZENE	5	H	1.25	0.1	ND	0.0125	ND	ND	ND	ND	ND	ND
BROMOFORM				ND	ND	ND	ND	ND	ND	ND	ND	ND
BROMOMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CARBON TETRACHLORIDE	5	H	1.25	ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROBENZENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROFORM				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CIS-1,3-DICHLOROPROPYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DIBROMOCHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
ETHYLENE DIBROMIDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
METHYLENE CHLORIDE				68.5	ND	9.7857	292	ND	41.714	ND	ND	ND
TETRACHLOROETHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
TRANS-1,2-DICHLOROETHYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
TRANS-1,3-DICHLOROPROPYLENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
TRICHLOROETHYLENE	50	H	12.5	0.3	ND	0.1	ND	ND	ND	ND	ND	ND
TRICHLOROFLUOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
VINYL CHLORIDE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,1,1-TRICHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
DICHLOROMETHANE	50	H	12.5	ND	ND	ND	ND	ND	ND	ND	ND	ND
CIS-1,2-DICHLOROETHENE				ND	ND	ND	ND	ND	ND	ND	ND	ND
BROMODICHLOROMETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
CHLOROETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND
1,2-DIBROMOETHANE				ND	ND	ND	ND	ND	ND	ND	ND	ND

ODWO Ontario Drinking Water Objective
(H – Health, A – Aesthetic, inter H – interim health)
RUP – Reasonable Use Policy Guideline
Calculated assuming background concentration equal to 0 µg/L

Table D2: Assessment of Critical Organic Contaminants

all concentrations in µg/L

Compound	ODWO			57-II, 58-I		
	Limit	Type	RUP	max	min	avg
MISA Group 20 – Acid Extractables						
2,3,4,5-TETRACHLOROPHENOL						
2,3,4,6-TETRACHLOROPHENOL	100	H	25	ND	ND	ND
2,3,5,6-TETRACHLOROPHENOL				ND	ND	ND
2,3,4-TRICHLOROPHENOL				ND	ND	ND
2,3,5-TRICHLOROPHENOL				ND	ND	ND
2,4,5-TRICHLOROPHENOL						
2,4,6-TRICHLOROPHENOL	5	H	1.25	ND	ND	ND
2,4-DIMETHYLPHENOL				ND	ND	ND
2,4-DINITROPHENOL				ND	ND	ND
2,4-DICHLOROPHENOL	900	H	225	ND	ND	ND
2,6-DICHLOROPHENOL				ND	ND	ND
4,6-DINITRO-O-CRESOL				ND	ND	ND
2-CHLOROPHENOL				ND	ND	ND
4-CHLORO-3-METHYLPHENOL				ND	ND	ND
4-NITROPHENOL				ND	ND	ND
M-CRESOL & P-CRESOL				1690	5	847.5
O-CRESOL				528	ND	264
PENTACHLOROPHENOL	60	A	30	ND	ND	ND
PHENOL				5970	292	3131
NITROPHENOL						
2-METHYL-4-6-DINITROPHENOL						
Misa Group 19 – Base/Neutral Extractables						
ACENAPHTHENE				33	ND	16.5
5-NITROACENAPHTHENE				ND	ND	ND
ACENAPHTHYLENE				ND	ND	ND
ANTHRACENE				17.5	ND	8.75
BENZ(A)ANTHRACENE				ND	ND	ND
BENZO(A)PYRENE	0.01	H	0.0025	ND	ND	ND
BENZO(B)FLUORANTHENE				ND	ND	ND
BENZO(G,H,I)PERYLENE				ND	ND	ND
BENZO(K)FLUORANTHENE				ND	ND	ND
BIPHENYL				ND	ND	ND
CAMPHENE				ND	ND	ND
1-CHLORONAPHTHALENE				ND	ND	ND
2-CHLORONAPHTHALENE				ND	ND	ND
CHRYSENE				ND	ND	ND
DIBENZ(A,H)ANTHRACENE				ND	ND	ND
FLUORANTHENE				22.1	ND	11.05
FLUORENE				25.4	ND	12.7
INDENO(1,2,3-CD)PYRENE				ND	ND	ND
INDOLE				ND	ND	ND
1-METHYL NAPHTHALENE				17.4	ND	8.7
2-METHYL NAPHTHALENE				23.1	ND	11.55
NAPHTHALENE				382	ND	191
PERYLENE				ND	ND	ND
PHENANTHRENE				43.3	ND	21.65
PYRENE				17.7	ND	8.85
BENZYL BUTYL PHTHALATE				ND	ND	ND
BIS(2-ETHYLHEXYL)PHTHALATE				ND	ND	ND
DI-N-BUTYL PHTHALATE				ND	ND	ND
DI-N-OCTYL PHTHALATE				ND	ND	ND
4-BROMOPHENYL PHENYL ETHER				ND	ND	ND
4-CHLOROPHENYL PHENYL ETHER				ND	ND	ND
BIS(2-CHLOROISOPROPYL)ETHER				ND	ND	ND
BIS(2-CHLOROETHYL)ETHER				ND	ND	ND
DIPHENYL ETHER				ND	ND	ND
2,4-DINITROTOLUENE				ND	ND	ND
2,6-DINITROTOLUENE				ND	ND	ND
BIS(2-CHLOROETHOXY)METHANE				ND	ND	ND
DIPHENYLAMINE & N-NITROSODIPHA				ND	ND	ND
N-NITROSODI-N-PROPYLAMINE				ND	ND	ND

ODWO Ontario Drinking Water Objective

(H – Health, A – Aesthetic, inter H – interim health)

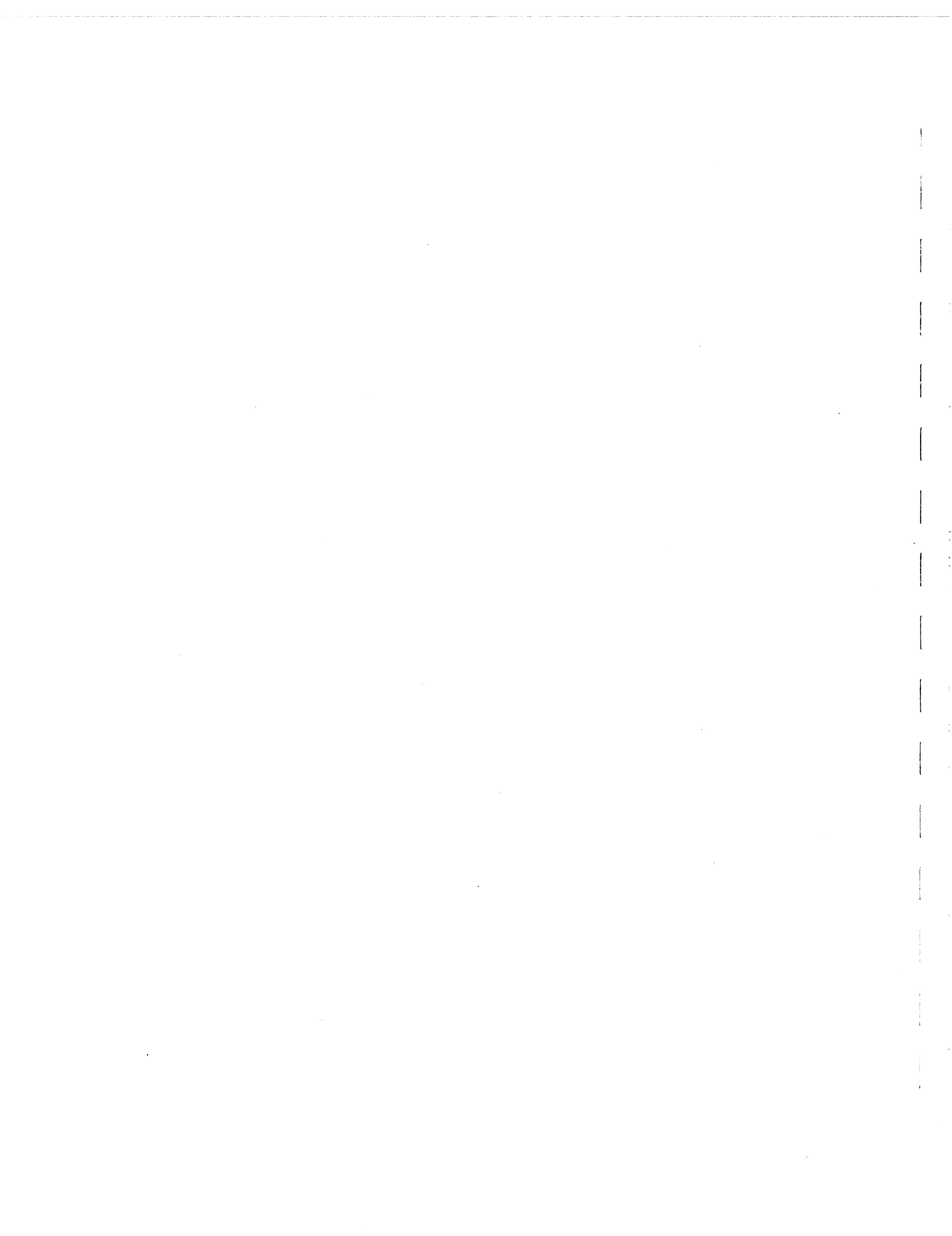
RUP – Reasonable Use Policy Guideline

Calculated assuming background concentration equal to 0 µg/L

Table D2: Assessment of Critical Organic Contaminants

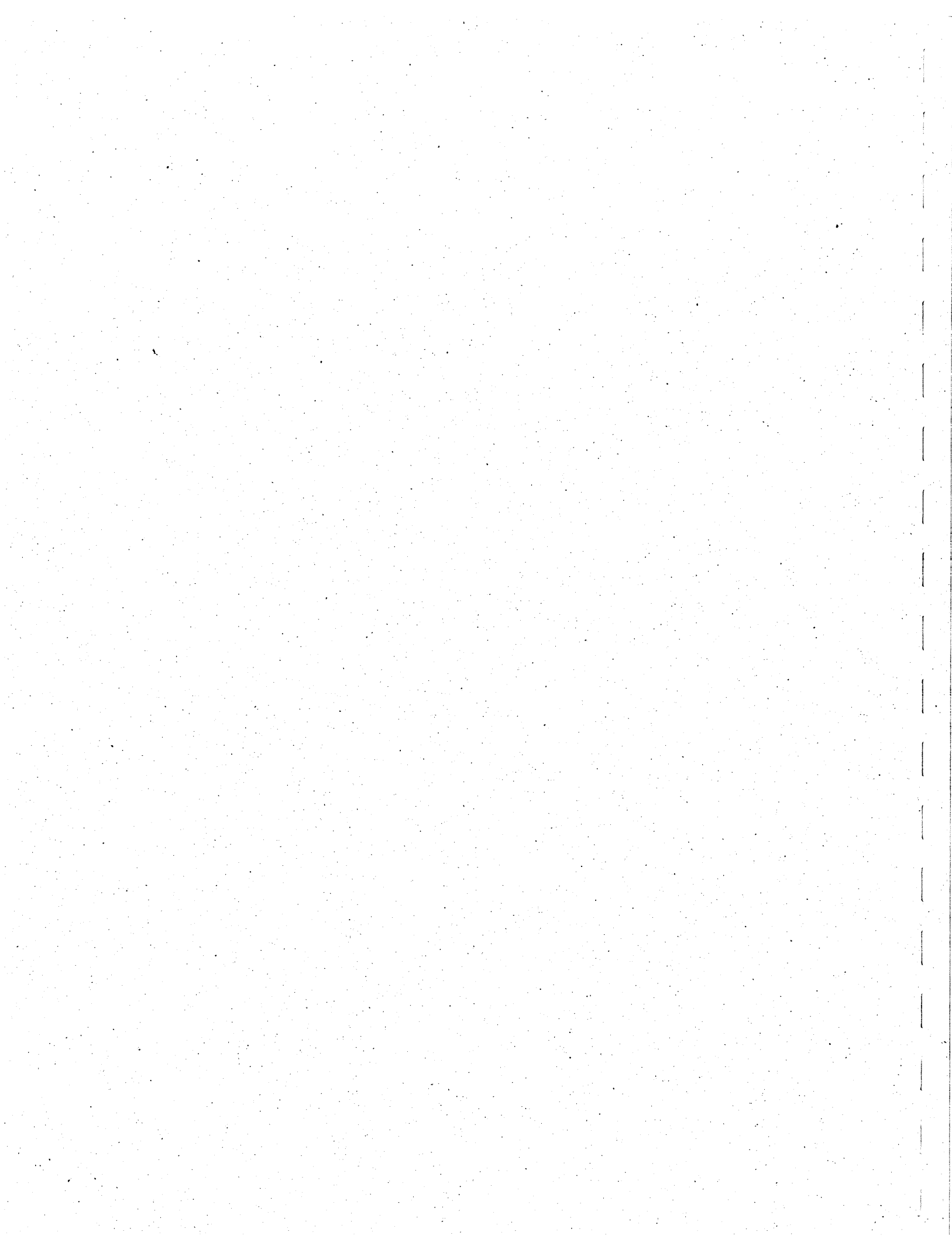
Compound	all concentrations in µg/L					
	ODWO			57-II, 58-I		
	Limit	Type	RUP	max	min	avg
MISA Group 22 – Organochlorine Compounds						
ALDRIN				0.003	ND	0.0015
DIELDRIN				ND	ND	ND
ALDRIN + DIELDRIN	0.7	H	0.175	0.003		
ALPHA-BHC				ND	ND	ND
BETA-BHC				ND	ND	ND
DELTA-BHC				ND	ND	ND
GAMMA-BHC				0.002	ND	0.001
CHLORDANE	7	H	1.75	ND	ND	ND
DDD				ND	ND	ND
DDE				ND	ND	ND
DDT	30	H	7.5	ND	ND	ND
2,4-DDT				ND	ND	ND
ENDOSULFAN I				ND	ND	ND
ENDOSULFAN II				ND	ND	ND
ENDOSULFAN SULPHATE				ND	ND	ND
ENDRIN				ND	ND	ND
ENDRIN ALDEHYDE				ND	ND	ND
HEPTACHLOR				0.006	0.002	0.004
HEPTACHLOR EPOXIDE				ND	ND	ND
HEPTACHLOR + HEPTACHLOR EPOXIDE	3	inter H	0.75	0.006		
METHOXYCHLOR	900	H	225	ND	ND	ND
MIREX				ND	ND	ND
TOXAPHENE				ND	ND	ND
PCB's	3	H	0.75	ND	ND	ND
MISA Group 17						
BENZENE	5	H	1.25	21.2	0.3	10.75
ETHYLBENZENE	2.4	A	1.2	5.5	ND	2.75
STYRENE				ND	ND	ND
TOLUENE	24	A	12	22.5	0.2	11.35
O-XYLENE	300	A	150	17.1	0.3	8.7
M-XYLENE + P-XYLENE	300	A	150	22.8	0.5	11.65
MISA Group 18						
ACROLEIN						
ACRYLONITRILE						
MISA Group 16 – Halogenated VOC's						
1,1,2,2-TETRACHLOROETHANE				ND	ND	ND
1,1,2-TRICHLOROETHANE				ND	ND	ND
1,1-DICHLOROETHANE				ND	ND	ND
1,1-DICHLOROETHYLENE				ND	ND	ND
1,2-DICHLOROBENZENE	200	H	50	ND	ND	ND
1,2-DICHLOROETHANE	5	inter H	1.25	ND	ND	ND
1,2-DICHLOROPROPANE				ND	ND	ND
1,3-DICHLOROBENZENE				ND	ND	ND
1,4-DICHLOROBENZENE	5	H	1.25	ND	ND	ND
BROMOFORM				ND	ND	ND
BROMOMETHANE				ND	ND	ND
CARBON TETRACHLORIDE	5	H	1.25	ND	ND	ND
CHLOROBENZENE				ND	ND	ND
CHLOROFORM				ND	ND	ND
CHLOROMETHANE				ND	ND	ND
CIS-1,3-DICHLOROPROPYLENE				ND	ND	ND
DIBROMOCHLOROMETHANE				ND	ND	ND
ETHYLENE DIBROMIDE				ND	ND	ND
METHYLENE CHLORIDE				ND	ND	ND
TETRACHLOROETHYLENE				ND	ND	ND
TRANS-1,2-DICHLOROETHYLENE				ND	ND	ND
TRANS-1,3-DICHLOROPROPYLENE				ND	ND	ND
TRICHLOROETHYLENE	50	H	12.5	ND	ND	ND
TRICHLOROFLUOROMETHANE				ND	ND	ND
VINYL CHLORIDE				ND	ND	ND
1,1,1-TRICHLOROETHANE						
DICHLOROMETHANE	50	H	12.5			
CIS-1,2-DICHLOROETHENE						
BROMODICHLOROMETHANE				ND	ND	ND
CHLOROETHANE						
1,2-DIBROMOETHANE						

ODWO Ontario Drinking Water Objective
 (H – Health, A – Aesthetic, inter H – interim health)
 RUP – Reasonable Use Policy Guideline
 Calculated assuming background concentration equal to 0 µg/L



Appendix E

**Water Budget
Estimate of Leachate Production**



WATER BUDGET WRITE-UP FOR HAMILTON AIRPORT

Long-term meteorological data for the Hamilton A meteorological station have been reviewed to prepare a water budget for this site.

It is estimated that the mean annual precipitation at Hamilton A is 890 mm per year, based on 31 years of meteorological data from 1959 to 1990. There is some variation, from year to year, in the total annual precipitation. It has been estimated that the total annual precipitation varies from 793 mm to 988 mm during 13 out of 20 years. This range is equivalent to a variation of one standard deviation of annual precipitation about the mean value.

The distribution of the precipitation varies from month to month, as shown on Figure D1 for a normal year.

A Water Balance has been prepared using the method described in Thornthwaite and Mather (1957). The mean annual evapotranspiration is estimated to be 552 mm, based on an assumed soil moisture storage of 100 mm (Figure D2). The mean annual water surplus is calculated to be 338 mm. The annual surplus is likely to range from 268 mm to 414 mm during 13 out of 20 years.

The distribution of the surplus water on a monthly basis through a normal year is shown on Figure D1. It shows that a significant surplus of 412 mm occurs during the autumn, winter and spring months and a deficit of 74 mm occurs during the summer.

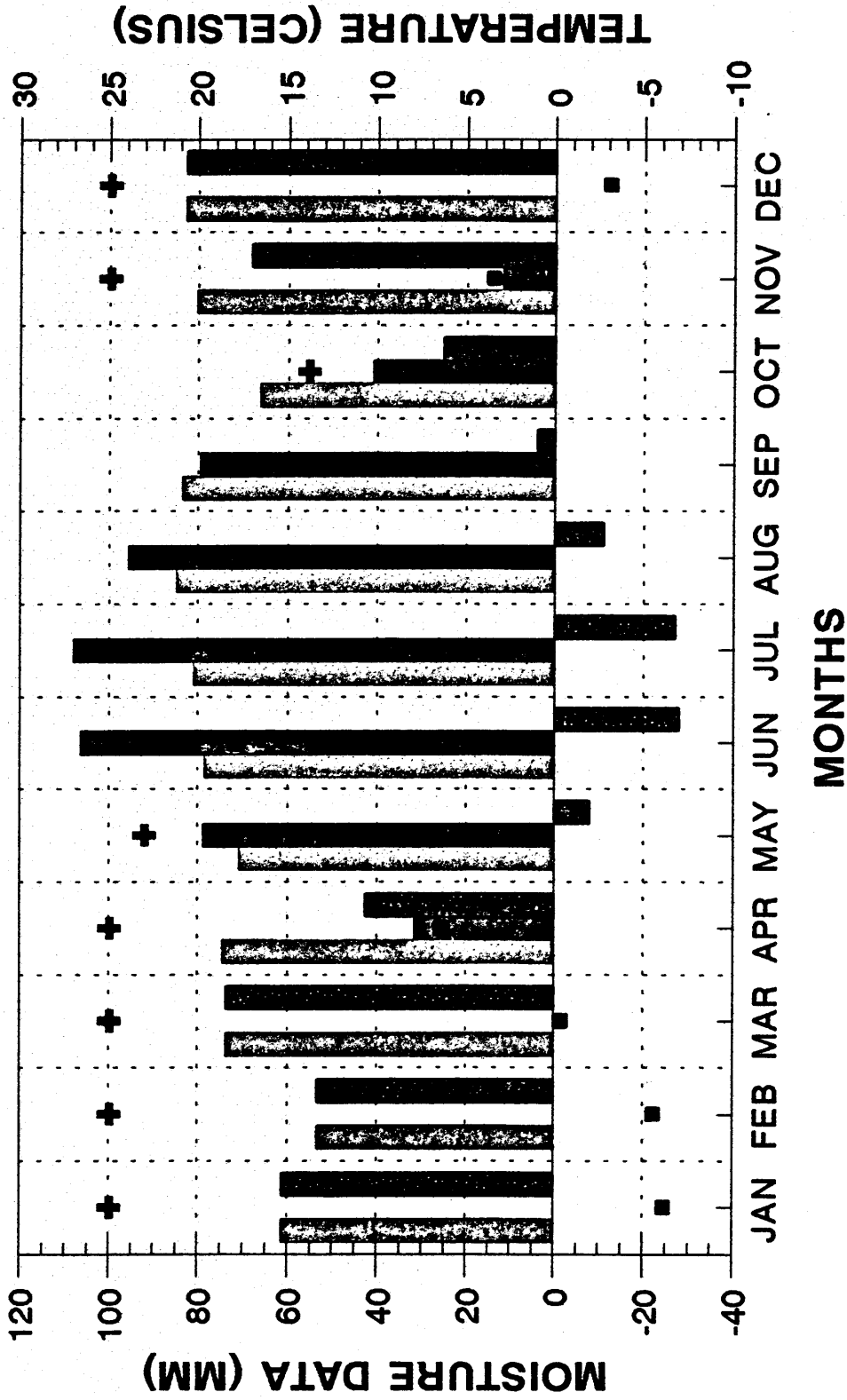
The water surplus includes both the surface runoff and infiltration components of a water balance. Site specific conditions like soils and topography need to be evaluated in order to partition the surplus.

Reference:

Thornthwaite C. W., and J. R. Mather:

1957 Instructions And Tables For Computing Potential Evapotranspiration And The Water Balance; Drexel Institute of Technology, Laboratory Of Climatology, Publications In Climatology, Volume X, Number 3, 1957, 311 pp.

FIGURE D.1 WATER BALANCE SUMMARY HAMILTON AIRPORT, 1959 - 1990



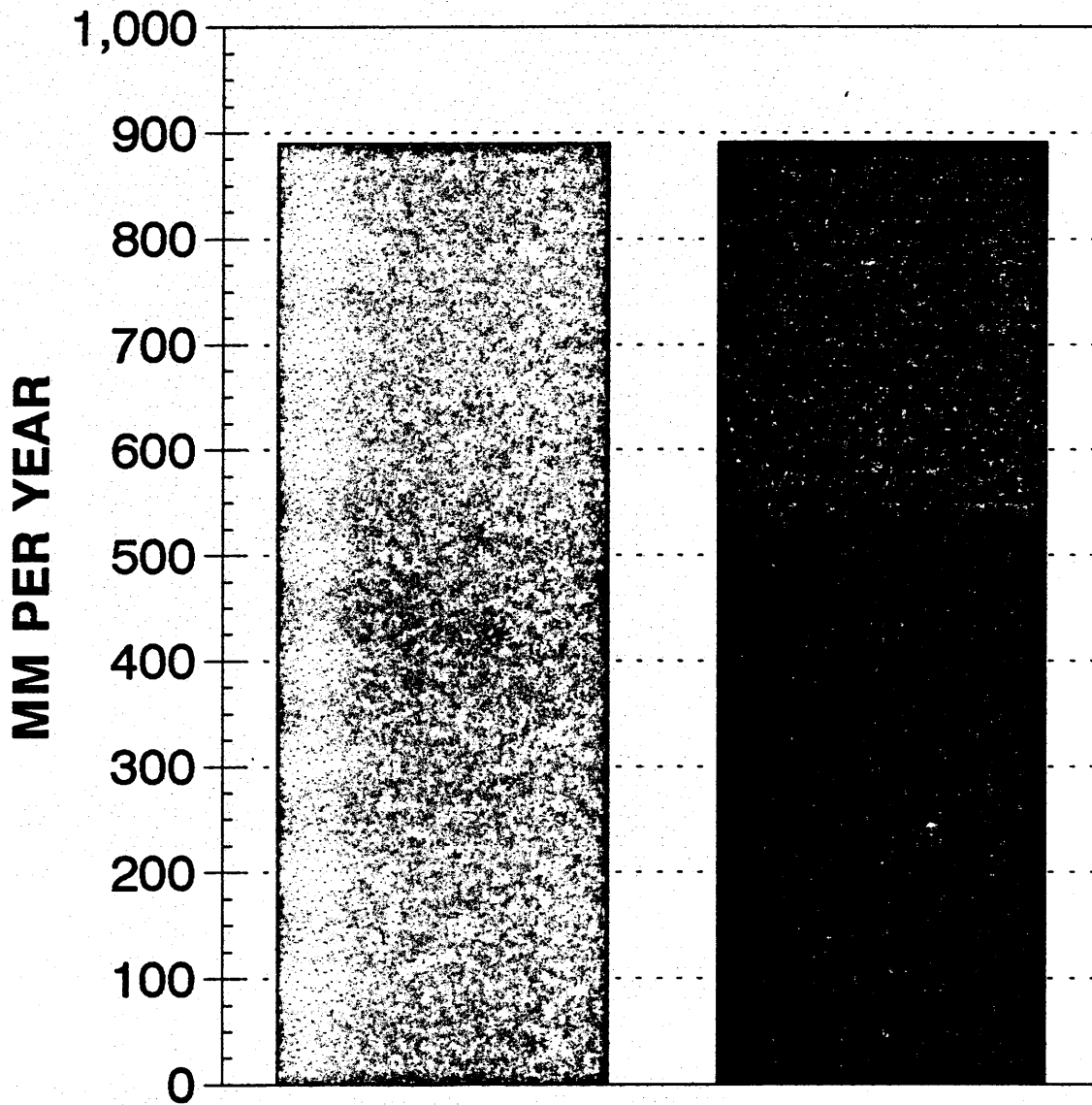
- PRECIPITATION
- SURPLUS WATER
- TEMPERATURE
- EVAPOTRANSPIRATION
- + SOIL MOISTURE

CALCULATED USING THORNTHWAITTE METHOD, ASSUMED SOIL MOISTURE CAPACITY: 100 MM
GLL 94-405, 191405/WATBUD1.CH3, JJPM, 94.03.24



FIGURE D.2

WATER BALANCE SUMMARY FOR HAMILTON AIRPORT, 1959 - 1990



COMPONENTS OF WATER BALANCE

 PRECIPITATION

 EVAPOTRANSPIRATION

 SURPLUS WATER

ESTIMATE OF LEACHATE PRODUCTION

Step 1:

Leachate will be produced at this site from the infiltration of rain or melt water into the wastes.

Assumptions

Water available for infiltration is calculated from the water budget presented in Appendix C. The average annual water surplus is 338 mm, or 0.338 m/a. This is based on the subtraction of actual evapotranspiration from the total precipitation.

Step 2: Open Cell

During active landfilling of a cell, it is assumed that the entire available surplus will infiltrate.

Therefore, the average rate of leachate production, per hectare, in an open cell can be calculated.

$$\begin{aligned} & 0.338 \frac{\text{m}}{\text{a}} \times 10,000 \frac{\text{m}^2}{\text{ha}} \\ = & 3,380 \frac{\text{m}^3}{\text{a ha}} \quad \text{or} \quad 0.107 \text{ L/s/ha} \end{aligned}$$

Step 3: Closed Cell

Once a cell is closed it will be capped with 0.85 m of compacted clay, plus 0.15 m of vegetated topsoil. In a weathered condition it is assumed that the cap will turn about 33% of the water surplus aside. (Experience shows that this figure can vary locally from 0 to 40 %) Hence 67% of the surplus will infiltrate, and therefore leachate production may be calculated as:

$$\begin{aligned} 0.67 \times 3,380 & = 2,250 \text{ m}^3/\text{a/ha} \\ & \text{or } 0.071 \text{ L/s/ha} \end{aligned}$$

Step 4: Estimated Average Leachate Production After Closure

Based on a 59.06 ha landfill footprint, the average annual leachate production after closure (covered) is:

$$\begin{aligned} & 2,250 \text{ m}^3/\text{a/ha} \times 54.2 \text{ ha} \\ = & 121,950 \text{ m}^3/\text{a} \\ \text{or} & 4.21 \text{ L/s} \end{aligned}$$

Step 5: Effect of Annual Fluctuations

The water budget states that, in 13 out of 20 years the annual surplus is likely to range from 0.268 m to 0.414 m. By factoring this range to the average annual surplus of 0.338 m, a range in leachate production is calculated.

$$Q_{\text{MIN}} = \frac{.268}{.338} \times 4.21 \text{ L/s} = 3.3 \text{ L/s}$$

$$Q_{\text{MAX}} = \frac{.414}{.338} \times 4.21 \text{ L/s} = 5.2 \text{ L/s}$$

Therefore, it can be expected that leachate production will range between 3.0 and 4.7 L/s after landfill closure.

Appendix F

Contaminating Lifespan Calculations

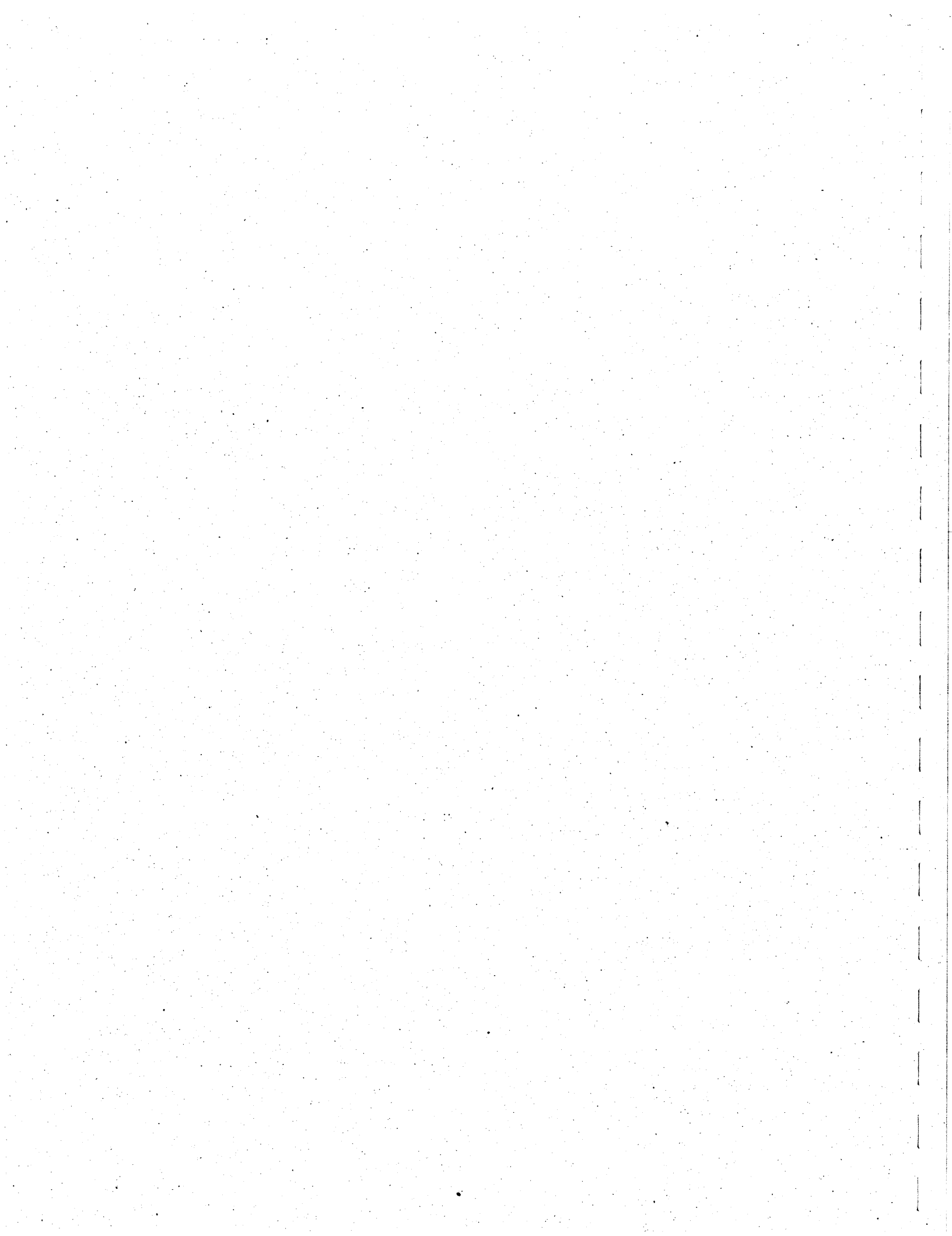


Table F1: Calculated Contaminating Lifespan in The Proposed East Quarry Landfill
 Method 1: Leachate concentration decays over time (Rowe, 1991)

Predicted mass of parameters in the waste

Data from bulk analysis March 1994	ELEMENTS kg	Sodium		Fluoride	
		mg/kg	mass of compound (mg)	mg/kg	mass of compound (mg)
Dofasco Waste					
Approved Mixed Waste	4,200,000,000	2510	1.05E+13	14	5.88E+10
Oxides	2,200,000,000	1338	2.94E+12	9	1.08E+10
other	200,000,000				
Industrial sands/dust/ashes	400,000,000				
Contaminated Soils	2,900,000,000	892	2.59E+12	5.5	1.80E+10
Misc Industrial Wastes	100,000,000				
Total	10,000,000,000				
Total mass of element in Landfill (mg) (% of total waste mass)		mg	1.61E+13 0.16%	mg	9.46E+10 0.0009%

(uses average bulk analysis concentration in each waste type)

Range in Critical Contaminant Concentrations

	Sodium (mg/L)	Fluoride (mg/L)
(1) Highest predicted East Quarry Landfill leachate concentration	739	3.9
(2) Average predicted East Quarry Landfill leachate concentration	629	2.4
(3) Highest observed concentration in the West Quarry leachate (mg/L) in areas with limited aluminum processing waste	552	3.9

Calculated Contaminating Lifespan

	Sodium	Fluoride
Parameter concentration considered acceptable for discharge (mg/L)	145 ODWO - a (based on RUP calculation)	0.9 ODWO - h (based on RUP calculation)
Time required to decrease the leachate concentration to levels considered acceptable for discharge to the environment using the highest predicted East Quarry Landfill leachate concentration	267	268
Time required to decrease the leachate concentration to levels considered acceptable for discharge to the environment using the average predicted East Quarry Landfill leachate concentration	282	291
Time required to decrease the leachate concentration to levels considered acceptable for discharge to the environment using the maximum leachate concentration in the West Quarry Landfill (mg/L) in areas with limited aluminum processing waste	293	268

$$t = -M \ln (C_L/C_0) / q A C_0$$

t = time at which the leachate concentrations have decreased enough to allow discharge to the environment

C₀ = Maximum Leachate Concentration

A = Landfill area (59.06 ha)

C_L = Leachate concentration required for discharge

M = Mass of contaminant

q = Infiltration rate (0.225 m/a)

RUP - Reasonable Use Policy for health parameters, RUP = background + .25 (ODWO - background)
 for aesthetic parameters, RUP = background + .5 (ODWO - background)

Estimated leachate production rate in East Quarry Landfill with Final Cover 0.225 m/a
 Based on long term average surplus rainfall of 0.336 mm/a, and 66% infiltration through the cover

Table F2: Calculated Contaminating Lifespan of the Proposed East Quarry Landfill

Calculation using mass balance model

Predicted Mass of Critical Contaminants using Bulk Analysis Information

ELEMENTS	Sodium		Fluoride	
	mg/kg	mass of compound (mg)	mg/kg	mass of compound (mg)
Data from Bulk analysis March 1994 (uses average concentrations)				
<u>Dofasco Waste</u>	kg			
Approved Mixed Waste	4,200,000,000	2510	14	5.88E+10
Oxides	2,200,000,000	1338	9	1.98E+10
other	200,000,000			
<u>Industrial sands/dust/ashes</u>	400,000,000			
<u>Contaminated Soils</u>	2,900,000,000	892	5.5	1.80E+10
<u>Misc Industrial Wastes</u>	100,000,000			
Total	10,000,000,000			
Total mass of element in Landfill (mg) (% of total waste mass)	mg	1.61E+13 0.16%	mg	9.46E+10 0.00%

Predicted Leachate Concentrations

	Sodium (mg/L)	Fluoride
(1) Highest predicted concentration in the East Quarry Landfill leachate	739	3.9
(2) Average predicted concentration in the East Quarry Landfill leachate	629	2.4
(3) Highest Observed Concentration in the West Quarry Leachate (mg/L) in areas with limited aluminum processing waste	552	3.9

Predicted Contaminating Lifespan for Critical Contaminants
Calculated from the Closure of the Proposed East Quarry Landfill

	Sodium	Fluoride
The total volume of water needed to leach out compound, using the highest predicted East Quarry Landfill leachate concentration	(L) 2.17E+10	(L) 2.42E+10
Calculated time required to leach out the element with leachate generation rate of 3.87 L/s	years 164	years 182
The total volume of water needed to leach out compound, using the average predicted East Quarry Landfill leachate concentration	(L) 2.56E+10	(L) 3.94E+10
Calculated time required to leach out the element with leachate generation rate of 3.87 L/s	years 192	years 297
The total volume of water needed to leach out compound, using the highest observed concentration in the West Quarry Leachate (mg/L) in areas with limited aluminum processing waste	(L) 2.91E+10	(L) 2.42E+10
Calculated time required to leach out the element with leachate generation rate of 3.87 L/s	years 219	years 182

Estimated leachate production rate in East Quarry Landfill with final cover (L/s) Based on long term average surplus rainfall of 0.338 mm/a, and a total area of 59.06 Ha Assumes 66% infiltration through the final cover	4.21 L/s
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2012 Construction Inspection Report – Newalta Stoney Creek Landfill Site Stage 1 Stormwater Management System



Newalta Corporation

2012 Construction Inspection Report – Newalta Stoney Creek Landfill Site Stage 1 Stormwater Management System

Prepared by:

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Project Number:

60265424

Date:

July, 2013

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July 31, 2013

Mr. Lorenzo Alfano
Newalta Corporation
65 Green Mountain Road
Stoney Creek, ON L8J 1X5

Dear Mr. Alfano:

Project No: 60265424

**Regarding: 2012 Construction Inspection Report – Newalta Stoney Creek Landfill Site
Stage 1 Stormwater Management System**

We are pleased to provide you with our report documenting the quality assurance work undertaken in 2012 for the Stage 1 Stormwater Management System. We understand that this report will be used to satisfy Condition 14.1 and 14.3 of Environmental Compliance Approval No. A181008 issued by the Ministry of the Environment (MOE) for the site. We note that a letter dated May 2, 2013 was submitted to the MOE immediately upon completion of the Stormwater Management System.

Please do not hesitate to contact us with any questions or comments.

Sincerely,
AECOM Canada Ltd.



Larry Fedec, P.Eng., M.BA.
Manager, Waste Services, Environment
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LMF:mm
Encl.

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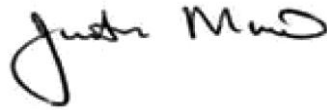
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1	1	Ministry of the Environment, Hamilton District Office
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AECOM Signatures



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1. Introduction

1.1 Background

Newalta Corporation operates the Newalta Stoney Creek Landfill (formerly the Taro Landfill) in Stoney Creek, Ontario. The site has been operating since December 1996 under Environmental Compliance Approval (ECA) No. A181008 issued by the Ministry of the Environment (MOE). Key conditions relating to the construction of the site’s Stage 1 Stormwater Management System are the following:

- **Condition 14.1:**
“Specifications and a detailed quality assurance/quality control program for construction of the Major works, and provisions for quality assurance procedures, with respect to the liner, to be undertaken by an independent third-party consulting firm, reporting to the Ministry.”
- **Condition 14.3:**
“The Company shall construct Major works in accordance with the approved final detailed design and shall implement the quality assurance procedures as approved by the Director.”



Braking and Hauling Rock from Forebay and Detention Pond Footprint

In 2012 Newalta undertook the construction of the Stage 1 Stormwater Management System which is shown in Figure 1. The main components of the Stage 1 Stormwater Management System include a perimeter drainage ditch along the west and south sides of the site which direct the stormwater into the forebay pond located at the northwest corner of the site. From the forebay pond the stormwater will flow through a 900 mm HDPE drainage pipe into the detention pond. Discharge from the detention pond is manually controlled by the outlet structure located at the northwest corner of the pond. The outlet structure consists of a 1,500 mm diameter concrete maintenance hole, fitted with a series 20-10c sluice gate. When the sluice gate is open, the stormwater will flow through a 750 mm drainage pipe to a 1,500 mm diameter concrete ditch inlet maintenance hole, and then into a culvert which runs under First Road West. This culvert discharges the stormwater into the road side ditch. Newalta retained AECOM to carry out the associated construction quality assurance work. The completion and documentation of this work satisfies Conditions 14.1 and 14.3.

Construction generally took place between July 2012 and April 2013, with the following being completed:

Construction generally took place between July 2012 and April 2013, with the following being completed:

- a) a perimeter drainage ditch was constructed around the south and west perimeter of the landfill site. A typical cross section through the perimeter ditch is shown on Figure 2.

- b) a forebay pond was constructed on the north side of the west site entrance road along First Road West
- c) A support berm was constructed from the forebay pond to the detention pond to support a 900 mm HDPE drainage pipe. This pipe allows the stormwater from the forebay pond to flow into the detention pond. A cross section through the support berm is shown on Figure 3.
- d) the detention pond was constructed on the north side of the site along Green Mountain Road, east of the forebay pond
- e) an overflow weir was constructed on the west side of the detention pond in order to direct excess stormwater to flow into the site's existing pond. A cross section of the overflow weir can be seen on Figure 4.
- f) An outlet structure consisting of a 1,500 mm diameter concrete maintenance hole, fitted with a series 20-10c sluice gate, was constructed within the detention pond to allow manual control of the stormwater discharge from the site to the road side ditch. A cross section through the outlet structures are shown on Figure 5.

The major components mentioned above are presented on Figure 6.

There were three (3) design changes from the original Stage 1 Stormwater Management System design. These design changes are listed below:

- a) The footprint of the detention pond has been reduced in area, from the original design, in order to keep a setback of 30 m from the existing septic bed. This reduction in footprint area has resulted in an overall reduction in storage capacity of approximately 35%.
- b) The one (1) 1,050 mm HDPE culvert originally designed to run under the site entrance road from First Road West was changed to three (3) 675 mm concrete culverts. As bedrock is at the surface in this area, this modification was made to reduce the amount of bedrock removal and fill required to provide cover for the 1,050 mm pipe. A cross section through the culverts is shown on Figure 7.
- c) Location of the 1,500 mm diameter concrete ditch inlet maintenance hole, and alignment of the 750 mm HDPE pipe from the detention pond were modified to match the existing location of the culvert running under First Road West.

A letter pertaining to completion of the Stage 1 Stormwater Management System was submitted to the MOE on May 2, 2013. Submission of this report constitutes the remainder of the required quality assurance documentation. A copy of the letter to the MOE is provided in Appendix A.

1.2 Scope of Report

This report is being submitted to the MOE in compliance with Condition 14.1 and 14.3 of the ECA No. A181008 for the Newalta Stoney Creek Landfill. It documents construction activities undertaken in 2012 and early 2013, and the associated construction quality assurance program. Photographs showing typical construction activities are shown in Appendix B. Daily documented construction activities can be seen in Appendix C.

The remainder of this report is organized as follows:

- a) Section 2 presents a brief overview of the construction activities;
- b) Section 3 summarizes the results of:
 - conformance testing of the materials used;
 - inspections to confirm that construction methods were achieved;
 - evaluation of the performance of the compacted clay liner;
 - conclusions
- c) Sections 4 provides a list of references.

Results of the various field and laboratory testing carried out during the Stage 1 Stormwater Management System work are presented in Appendices D through G of this report.

2. Construction Activities

2.1 Overview

Dufferin Construction Company (Dufferin) was contracted to complete the construction of the stormwater pond and related structures. Terrafix Environmental Technology Inc. (Terrafix), was responsible for the supply of the geotextile and geoweb used during construction.

Construction commenced on June 26, 2012 and concluded on April 30, 2013. Work was typically carried out Monday to Friday, between the hours of 7:00 a.m. to 5:00 p.m. (except during or immediately after periods of inclement weather). Construction, testing and inspection work was extended into weekends periodically to take advantage of good weather conditions, with the approval of the District MOE office.

2.2 Key Contractors

The key contractor involved in the construction of the Stage 1 Stormwater Management System, as well as their various roles and responsibilities are outlined in Table 1.

Table 1. Roles and Responsibilities of Key Contractor

Company	Role	Responsibilities
Dufferin Construction Company	General Contractor	• Construction of all components

2.3

Materials

The main suppliers and manufacturers of materials involved in the construction of the Stage 1 Stormwater Management System are outlined in Table 2.

Table 2. Suppliers and Manufacturers of Key Construction Materials

Material(s)	Supplier	Manufacturer(s)
Soil	Newalta Corporation	-
Granular	Newalta Corporation	Vinemount Quarries
Type 400-R Geotextile	Terrafix Geosynthetics Inc.	Propex Inc.
Terrafix Terraweb 200 mm	Terrafix Geosynthetics Inc.	Texel Inc.
HDPE BOSS 2000 Pipe	Sandale Utility Products	Oxford Plastics Inc.
HDPE DR35	Sandale Utility Products	Oxford Plastics Inc.

2.4

Construction Equipment

Major equipment employed during construction consisted of the following:

- a) **Tracked Excavators (Caterpillar 330C, 345CL, 365C, 550LC, John Deere 230LC, 350D, 450D)**
 - excavation and loading of soils and granular pipe bedding
 - bedrock excavation within detention pond (when equipped with a hydraulic hoe-ram)
 - compaction of pipe bedding (equipped with hoe-pack)
 - excavation of perimeter drainage ditch and pipe trenches
 - transport and support of large, heavy construction materials (e.g., geotextile rolls, concrete maintenance structures and piping.
 - Loading stone into gabion baskets and placing rip-rap.
- b) **Caterpillar D6N, John Deere 750J Bulldozers**
 - Spreading and shaping soils for clay liner and engineered fill
 - Spreading topsoil for the ponds
 - fine grading of ponds and ditches
- c) **Volvo A35, A30D, John Deere 350D Rock Trucks**
 - haulage of clay soils and granular materials
 - haulage of excavation spoil
- d) **Water Tank Trucks with Spray Hoses**
 - addition of water to clay soils or granular materials prior to compaction
 - application of water to haul roads for dust control
- e) **Bomag BW213PDH-3, Caterpillar CP563D Pad Foot Compactors**
 - compaction of engineered fill and clay liner for ponds and support berm
- f) **Terex “Zoom-Boom” Telescopic Fork-Lift**
 - movement of geotextile rolls

Other minor equipment used included diesel pumps, hand-guided augers and plate tampers/jumping jacks and skid steer.



Construction of Gabion Walls within Detention Pond

3. Construction Inspection and Testing

3.1 Overview

The benchmark for the quality assurance program was the approved Design Drawings and Specifications. Minor modifications to the design and quality assurance protocols were occasionally made in the field in order to accommodate specific site conditions. All such changes are documented in this report.

AECOM staff was on site to carry out quality assurance inspection and field testing during construction of the Stage 1 Stormwater Management System. AECOM carried out inspection and testing for the clay liner and engineered fill used in the forebay and detention ponds support berm, as well as the perimeter drainage ditch, maintenance hole structures and drainage pipe installation. AECOM and Dufferin jointly carried out surveying to check proper alignment and grade control in addition to the Global Positioning Satellite (GPS) grading hardware utilized on select Dufferin earth moving equipment.

In addition to the testing and inspection discussed herein, AECOM also carried out routine contract administration duties, and recorded the contractor’s activities in daily field inspection records.

3.2 Construction Materials Testing

3.2.1 Liner Soils

Soil used for the forebay and detention pond’s clay liner construction was obtained from on-site stockpiles and quarry overburden strippings. Soil used in the construction was routinely tested for basic geotechnical properties

including standard proctor density and optimum moisture content, Atterberg limits, and grain size analysis. Soil testing results are provided in Appendix D to F.

3.2.2 Engineered Fill

Engineered fill was used for construction of the forebay and detention pond base and sidewalls. The engineered fill was obtained from material excavated out of the perimeter drainage ditch and on site stockpiles. Engineered fill used in construction was routinely tested for standard proctor density and optimum moisture content. Test results for the engineered fill are provided in Appendix D and G.

3.2.3 Granular 'A'

Granular 'A' was used for the foundation pad of the manhole structure within the detention pond, for pipe bedding, and for various other minor applications. Granular 'A' used in the construction of the Stage 1 Stormwater Management System was imported from Vinemount Quarries.

3.2.4 Rip-Rap

Rip-Rap was placed at each bend within the perimeter drainage ditch, at the inlets of the forebay and detention ponds and around the perimeter of the overflow weir to prevent erosion due to the stormwater flow. Rip-rap was also used to construct the gabion walls inside the forebay and detention pond. The rip rap used in the Stage 1 Stormwater Management System was obtained from a previously produced onsite stockpile.

3.2.5 Clear Stone

50 mm clear stone was used as infill for the geoweb at the overflow wire of the detention pond. Clear stone used in construction of the Stage 1 Stormwater Management System was obtained from on-site stockpiles of product imported from Vinemount Quarries.

3.2.6 Geotextiles

Type 400-R geotextile was placed beneath the rip-rap at the inlet of the forebay and detention pond to protect the clay liner. Geoweb cellular system was used to construct the overflow weir located on the east edge of the detention pond.



Deployment of Geoweb

3.2.7 HDPE Pipes

Approximately 85 m of 900 mm diameter BOSS 2000 HDPE piping was installed to convey stormwater from the forebay to the detention pond. The 900 mm HDPE piping was placed within a trench excavated in the support berm, and buried following completion.

Approximately 95 m of 750 mm diameter HDPE piping was installed from the outlet structure within the detention pond to the ditch inlet manhole located at the east side of First Road West.

3.2.8 Concrete Structures

A 1,500 mm diameter concrete maintenance hole outlet structure was installed within the detention pond. The maintenance hole is fitted with a series 20-10c sluice gate to allow manual control of stormwater being discharged off-site.

A second 1,500 mm concrete ditch inlet maintenance hole was installed to replace the existing catch basin structure located at the corner of First Road West and Green Mountain Road. The east inlet pipe is a 750 mm diameter HDPE drainage pipe which comes from the outlet structure in the detention pond. The west outlet pipe is a 760 mm diameter CSP culvert which runs underneath First Road West and discharges into the road side ditch.

3.3 Construction Methods Inspection and Testing

3.3.1 General

The benchmark for the construction methods inspection and testing program was the approved Stage 1 Stormwater Management System detailed Design Drawings and Specifications.

Prior to construction of the Stage 1 Stormwater Management System, the following site preparations were necessary:

- “brush” area within the footprint of the detention pond was removed prior to the start of construction.
- clearing of stored materials from the work area
- the topsoil was stripped from the footprint area of the forebay pond and detention pond
- any bedrock outcrops within the construction area were broken and removed
- heightening and relocation of the overhead power line within the work area.

3.3.2 Engineered Fill

Engineered fill was used to construct the base and sidewalls of the forebay and detention pond. Soil conditioning prior to compaction was carried out in

the forebay / detention pond construction area and included rock and debris removal, breaking up of soil clods, and moisture adjustment. Water was added as required using a tank truck equipped with a spray canon.

Inspection and testing during the engineered fill placement generally consisted of:

- a) visual inspection of on-site soil stockpiles of the materials for construction and conditioning operations;
- b) visual inspection of the finished subgrade prior to engineered fill placement;
- c) visual inspection of methods used during compaction of each lift;
- d) in situ density and moisture content measurements using a nuclear density gauge, readings were periodically verified/ corrected by oven moisture content analysis on soil samples collected from in situ test locations; and
- e) Visual inspection of effects of the compaction and hauling equipment on the lifts.

The inspection was undertaken by AECOM staff, and the results of the dry density and moisture content testing are presented in Appendix G. In this appendix each test carried out is numbered sequentially and the test location is identified. In many cases, a given area of the ponds is represented by several tests where the first shows inadequate compaction and subsequent tests confirm that the required density was achieved following additional compaction.

The compaction and moisture content specifications for the engineered fill soil requires that each lift be compacted to at least 95% of SPD with moisture content within 2% of optimum water content. Test results are summarized as follows:

- a) densities and moisture contents within the desired range were routinely achieved; and
- b) in isolated cases density or moisture content measurements outside of the desired range were accepted, based on the observed appearance and handling characteristics of the soil. This was done in cases where the measurement was made in an area where the soil was re-moulded, where it was known that an adequate number of compactor passes were made (based on the number of passes required to reach the required density in adjacent areas) and where the moisture condition was visually similar to surrounding areas. Such judgements were made on a case-by-case basis by the AECOM soils inspector.

3.3.3

Clay Liner

Inspection and testing during clay liner construction consisted of the following:

- a) visual inspection of on-site soil stockpiles of the materials for construction and conditioning operations;



Perimeter Ditch with Culverts under the East Site Entrance Road

- b) visual inspection of the finished subgrade prior to clay liner construction;
- c) visual inspection of methods used during compaction of each lift;
- d) in situ density and moisture content measurements using a nuclear density gauge, readings were periodically verified/corrected by oven moisture content analysis on soil samples collected from in situ test locations;
- e) laboratory determinations of basic geotechnical properties and in situ moisture contents;
- f) laboratory and in situ hydraulic conductivity testing;
- g) visual inspection of action of the compaction and hauling equipment on the lifts,
- h) visual inspection of the finished surface of the clay liners;

The results of the *in situ* density and moisture content testing are presented in Appendix F. In this appendix each test carried out is numbered sequentially and the location identified (lift number, co-ordinates). In many cases, a given area of liner is represented by several tests, where the first test shows inadequate compaction and subsequent tests confirm that the required density was achieved following additional compaction. Probe holes created by the nuclear testing gauge were routinely filled with dry granular bentonite.

In situ moisture contents for the completed liner were determined by oven drying samples in the on-site laboratory and by nuclear gauge testing. Moisture contents obtained from oven drying averaged approximately 2% higher than the moisture contents obtained from nuclear gauge testing. This can likely be attributed to factors such as the position of the probe or the presence of foreign material below the surface (e.g., rocks) that can affect the accurate measurement of the *in situ* moisture content. In cases where the moisture contents obtained from the two methods differed by more than 2%, a moisture correction factor was applied to the nuclear gauge in order to correlate the field readings with those obtained from oven drying in the on-site laboratory. *In situ* moisture content results are provided in Appendix E.



HDPE Drainage Pipe Connecting the forebay pond to the detention pond

The compaction and moisture content specification for the clay liner requires that each lift of the liner be compacted to at least 98% of SPD with a moisture content within 1% to 3% wet of optimum moisture content. At the discretion of the Engineer, the Specifications allow the reduction of the required compaction density from 98% to 95% of SPD with a corresponding increase of the moisture content from 1% to 3% wet of the optimum moisture. The results of the *in situ* testing can generally be summarized as follows:

- a) densities and moisture contents within the desired range were routinely achieved; and
- b) in isolated cases density or moisture content measurements outside of the desired range were accepted based on the observed appearance and handling characteristics of the soil. This was done in cases where the measurement was made in an area where the soil was well re-moulded, where it was known that adequate compactor passes were made (based on the number of passes required to reach the required density in adjacent areas) and where the moisture condition was visually similar to surrounding areas where *in situ* measurements were within the range. Such judgments were made on a case-by-case basis by the AECOM soils inspector.

3.3.3.1

Construction Method

The first (i.e., lowest) lift of each clay liner was typically constructed with a lift thickness of approximately 250 mm. This thickness ensured that the underlying materials were not disturbed by the kneading action of the sheepsfoot compactor. The remaining lifts for each liner were typically constructed with an average compacted lift thickness of 200 mm. The clay liner in each the forebay and detention pond was constructed in three (3) lifts. The top lift of the clay liner was also typically overbuilt by about 50 mm and then cut down to the required grade and smooth rolled. This reduced productivity losses in the event of rainfall since only the 'overbuilt' surficial soils would typically be affected and could be rapidly removed.

Soil conditioning prior to compaction was carried out at the forebay / detention pond construction area and included rock removal, breaking up of soil clods, and moisture adjustment. Water was added as required using a tank truck equipped with a spray canon. Excessively wet soils were spread, broken up and allowed to air dry.

The removal of debris/rock from stockpiled soils was carried out routinely by Dufferin during the clay placement.

3.3.4

Geotextile and Geoweb Installation

Visual inspections were carried out during all aspects of geotextile and geoweb installation to ensure that:

- a) the material was not damaged during handling or placement;

- b) material was covered with overlying rip-rap or 50 mm clean stone in a timely manner (e.g., within about four weeks) to prevent ultraviolet light damage to the fabric;
- c) when the geotextile was overlapped, a minimum 600 mm overlap was used.

The geotextile and geoweb products were generally placed by hand. Torn or punctured material was either patched with sufficient overlap to prevent separation or replaced. Geoweb was secured in place using manufacturer supplied pins, or 8 inch spikes. Geoweb was filled with 50 mm clear stone once a sufficient area was completed. In order to prevent wind damage to the geotextile, sand bags were placed along the edges immediately following deployment, until the overlying materials could be placed.

3.3.5 Piping Installation

Various pipe sizes of concrete, HDPE, and PVC were used during construction of the Stage 1 Stormwater Management System. Visual inspections were carried out during all aspects of piping installation to ensure that:

- a) materials were not damaged during handling or placement;
- b) granular bedding was placed and compacted according to specifications prior to installing piping
- c) elevations were verified to ensure proper inverts, flow and pipe alignment were achieved
- d) required gaskets, couplings and other components were installed according to manufactures specifications

3.3.6 Concrete Maintenance Holes

Two precast concrete maintenance holes were installed as part of the Stage 1 Stormwater Management System. Inspections were carried out during all aspects of installation to ensure that:

- a) materials were not damaged during handling or installation;
- b) granular bedding was placed to appropriate thickness and compacted prior to setting the manhole base;
- c) elevations were verified to ensure proper inverts, flow and pipe alignment were achieved;
- d) required gaskets and other components were installed according to manufactures specifications.

3.3.7 Perimeter Drainage Ditch

Approximately 1,300 m of perimeter ditch was excavated to collect stormwater runoff from the site and direct the flow to the forebay and

detention pond. Inspections were carried out during all aspects of ditch construction to ensure that:

- a) proper alignment and grades were being achieved;
- b) existing trees, cleanout structures, etc., were avoided where possible;
- c) elevations were verified to ensure proper inverts;
- d) geotextile and rip rap was placed as specified.

3.4 Conclusions

The following conclusions are drawn from the results of the quality assurance work undertaken during the 2012 Stage 1 Stormwater Management System:

- a) quality assurance work was carried out by AECOM during Stage 1 Stormwater Management System construction. The quality assurance protocols were in general conformance with those described in the approved specifications. Based on this work, it is concluded that the Stage 1 Stormwater Management System has been constructed in general conformance with the approved final detailed design;
- b) some modifications were made to the design of temporary works and quality assurance protocols to accommodate field conditions and material characteristics. We consider that these do not deviate from the intent of the design, and are not expected to have any effect on control system performance; and

4. References

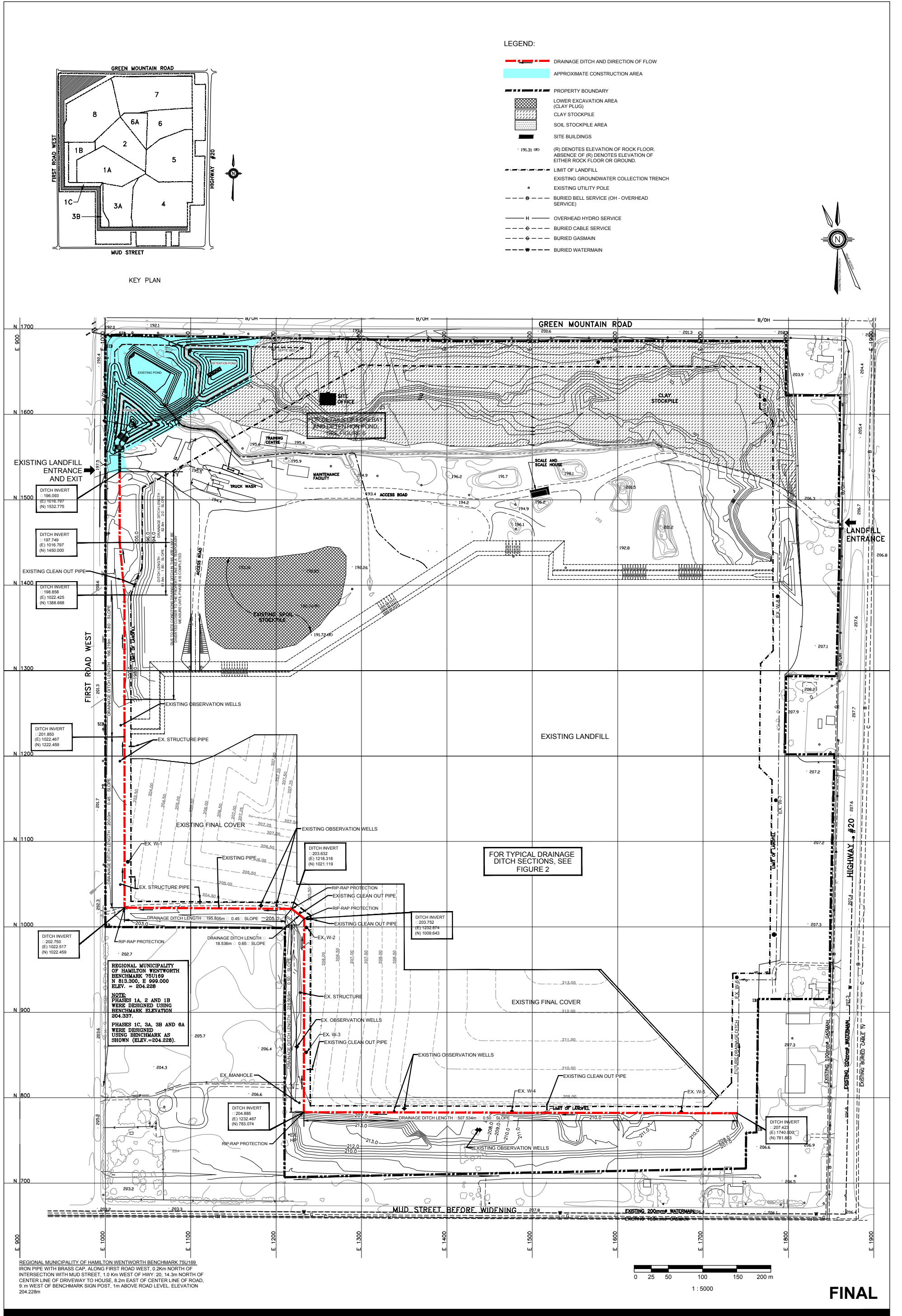
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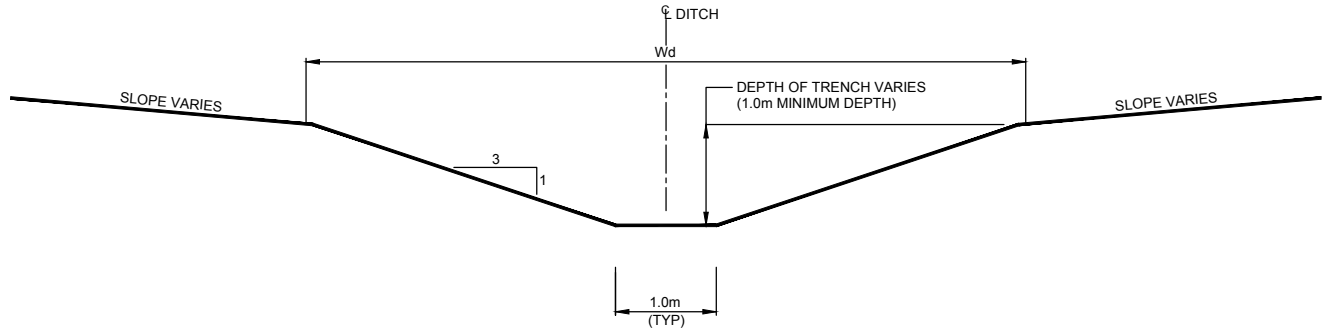
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Figures

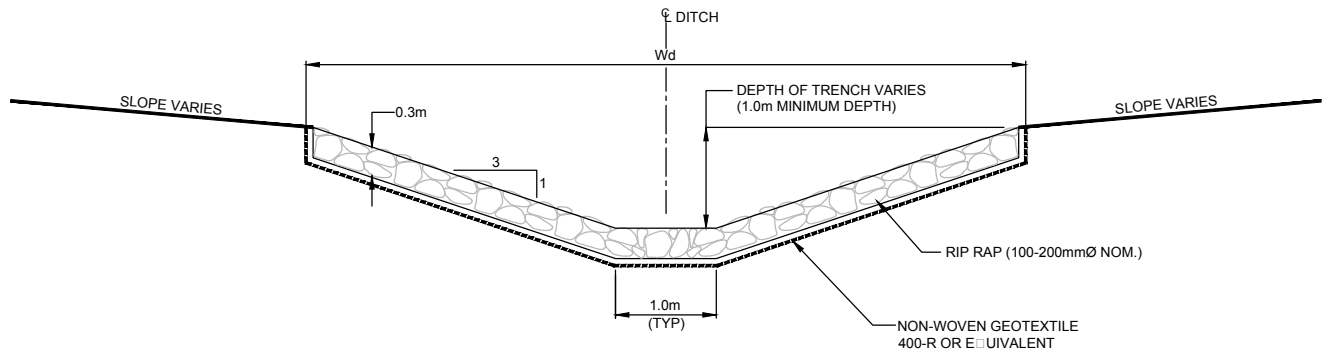


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TYPICAL DITCH CROSS SECTION

scale □ N.T.S.

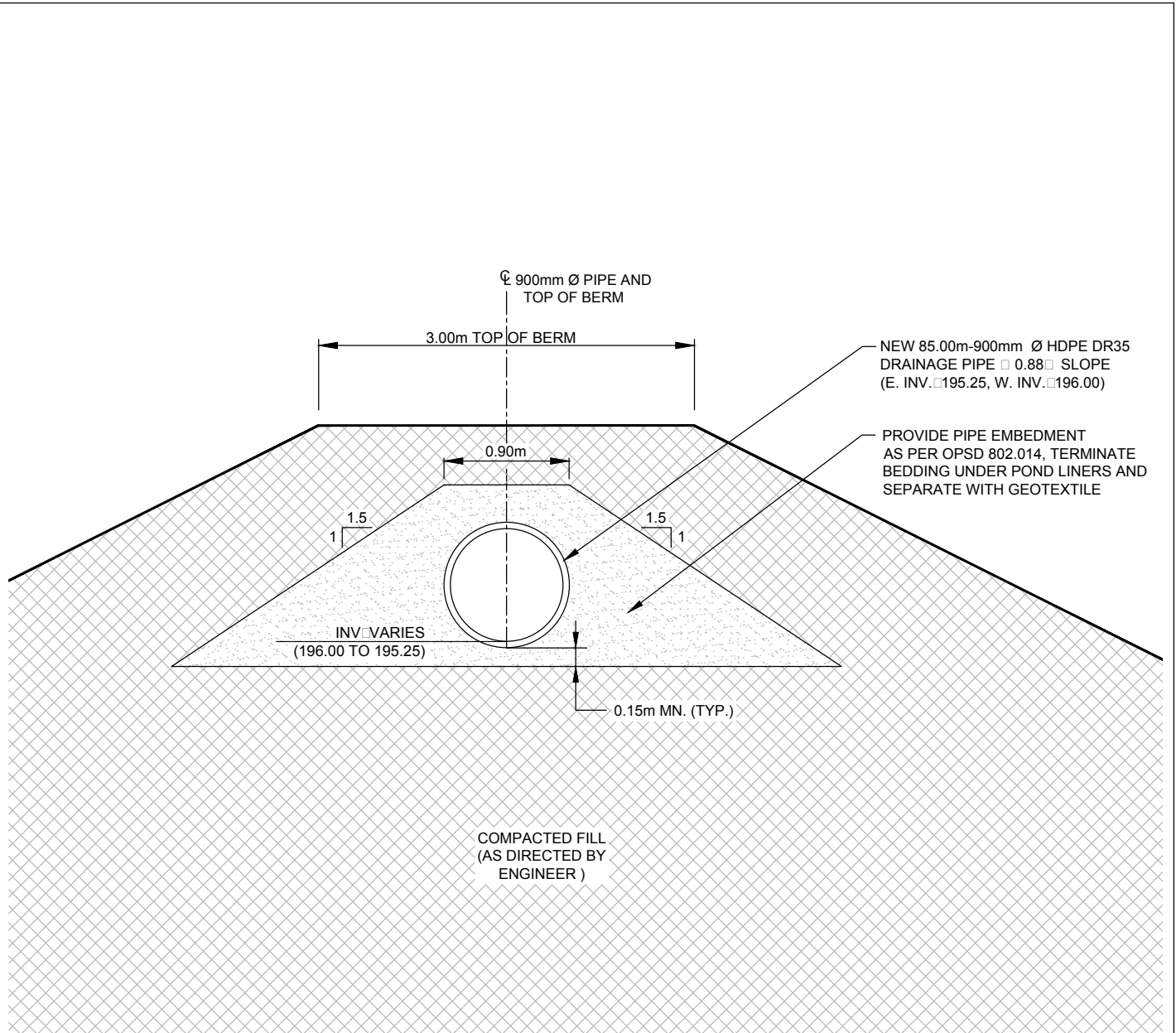


TYPICAL DITCH CROSS SECTION WITH RIP-RAP TREATMENT

scale □ N.T.S.

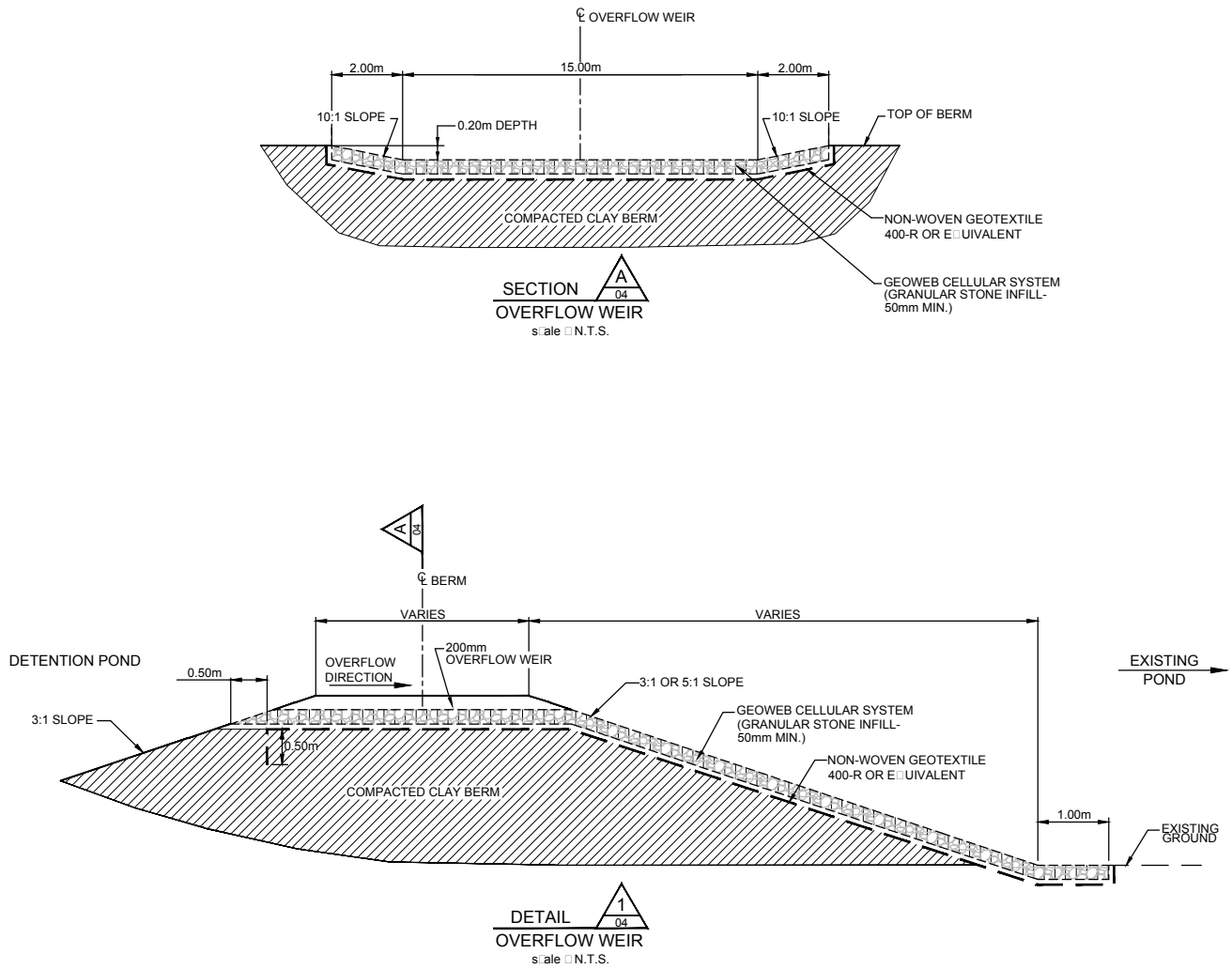
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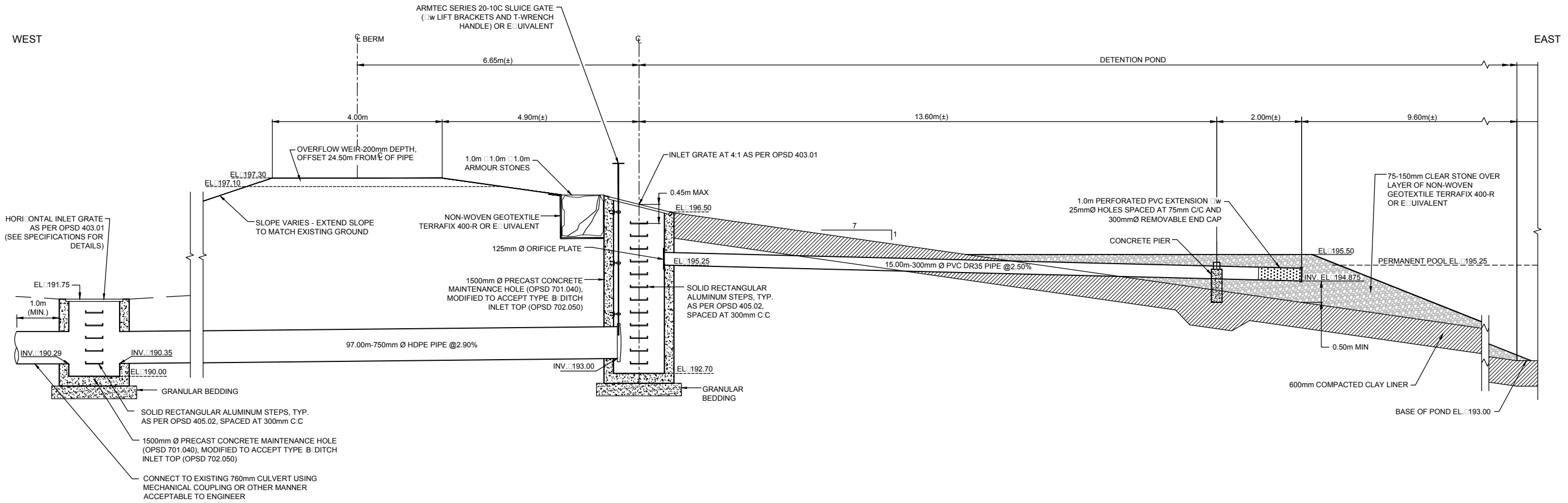


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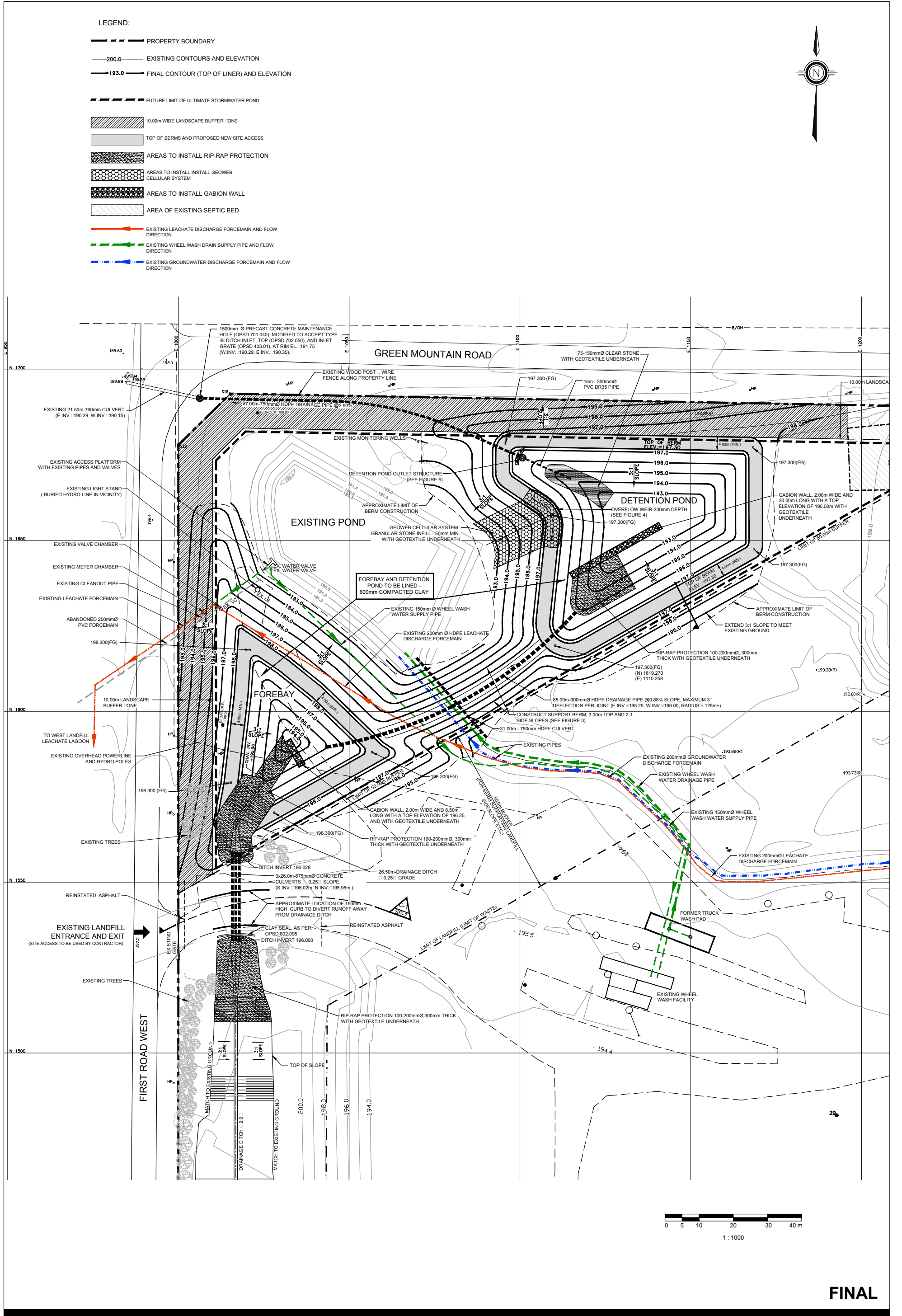


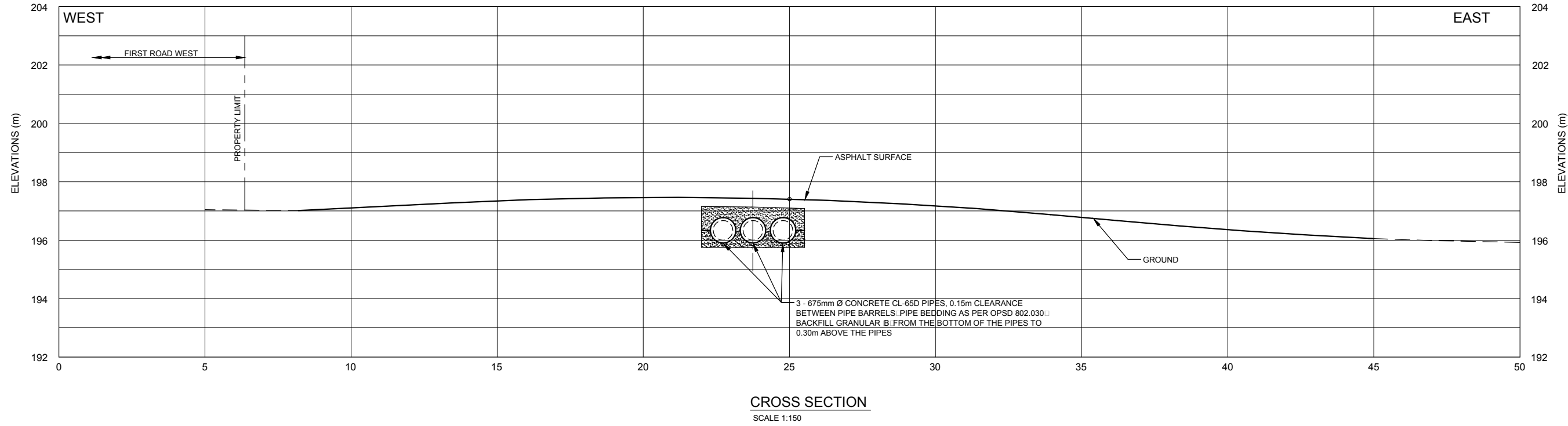
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CROSS SECTION THROUGH
OUTLET STRUCTURE





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CROSS SECTION THROUGH
THE CULVERT UNDER THE
WEST SITE ENTRANCE

Appendix A

Letters to Ministry of the
Environment

May 2, 2013

Mr. Bill Bardswick
Director, Hamilton Regional Office
Ministry of the Environment
119 King Street West
12th Floor
Hamilton, Ontario
L8P 4Y7

Dear Mr. Bardswick:

Project No: 60265424

Regarding: Completion of Stage I Stormwater Management Facility, Newalta Landfill, Stoney Creek, Ontario (Industrial Sewage Works Environmental Compliance Approval No. 5400-7DSSHU)

Herein we provide our opinion that the construction of the stormwater management ponds and perimeter drainage ditches for the Stage I Stormwater Management Facility (SMF) at the Newalta Stoney Creek Landfill has been principally completed. The following is relevant:

- a) Construction of the forebay, detention pond, overflow weir, and drainage structures have all been completed in the northwest corner of the site.
- b) Perimeter drainage ditch construction has been completed over approximately 1,450 metres along the south and west sides of the landfill.
- c) Quality assurance inspection has been carried out by AECOM Canada Limited, including overall contract administration, general construction oversight, and soil compaction testing. Based on this inspection work, we are of the opinion that the SMF has been constructed in general accordance with the approved design and specifications.
- d) We understand that Newalta will commence operation of the SMF following implementation of the approved monitoring program and the submission of a *Stormwater Contingency and Remedial Action Plan*. Upon completion of these tasks, the SMF will be operated in a normally open position and uncontaminated stormwater will be discharged from the site to the roadside ditch outletting to Davis Creek.

We will provide detailed documentation of the construction and quality assurance work upon its full completion. Should you have any questions, please do not hesitate to contact the undersigned, or Mr. Lorenzo Alfano of Newalta at (905) 548-5876.

Sincerely,
AECOM Canada Ltd.



Brian Dermody, P. Eng.
Environmental Engineer
brian.dermody@aecom.com
D: 905-477-8400 x384

BMD
cc: Mr. Lorenzo Alfano, Newalta Corporation
Mr. Geoffrey Knapper, MOE District Manager

Appendix B

Construction Photographs



Photograph 1. Breaking and Removing Bedrock within Forebay and Detention Pond Footprint ↑



Photograph 2. Compacting Clay Liner within Forebay Pond ↑



Photograph 3. Construction of Gabion Wall within Detention Pond ↑



Photograph 4. Installation of Geoweb for the Overflow Weir ↑



Photograph 5. Construction of the HDPE Drainage Pipe from the Forebay to the Detention Pond ↑



Photograph 6. Installation of Maintenance Hole at the Corner of Green Mountain Rd and First Rd ↑



Photograph 7. Installation of Maintenance Hole with Detention Pond ↑



Photograph 8. Construction of Perimeter Drain Ditch ↑



Photograph 9. Culverts under the West Site Entrance ↑



Photograph 10. Detention Pond ↑



Photograph 11. Forebay Pond ↑

Appendix C

Daily Activity Logs

Field Inspection Record

Job Number: 60265424 **Date:** June 27, 2012

Client: Newalta Corporation

Job Name: Stormwater Management System / 7A Cell

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Overcast/25°C/ cool breeze/afternoon rain

progress:

**Detention/
Forebay Pond**

- Stripped topsoil from the North limit of landfill within detention pond footprint.
- Constructed ramp to the north limit of the landfill for brush removal and clay excavation.
- Began excavating clay from the north limit of the landfill.
- Stock piled excavated clay on the east side of the detention pond footprint.
- Started layout for perimeter drainage ditch south of the west entrance.
- AECOM took clay sample from north limit of landfill (within detention pond footprint) – sample sent to Terraprobe.

Field Inspection Record

Job Number: 60265424 Date: June 28, 2012

Client: Newalta Corporation

Job Name: Stormwater Management System / 7A Cell

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny, warm (30°C), slight breeze

progress:**Detention/
Forebay Pond**

- Excavating clay from the north limit of the landfill.
- Stock piling excavated clay on the east side of detention pond footprint.
- Started layout for forebay pond construction.
- Removed top soil from the forebay pond footprint and stockpiled it outside of the footprint.
- Excavated the forebay pond to correct base grade elevation.

Field Inspection Record

Job Number: 60265424 Date: June 29, 2012

Client: Newalta Corporation

Job Name: Stormwater Management System/ 7A Cell

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny, Warm (30°C), slight breeze

progress:**Detention /
Forebay Pond**

- Started excavation of perimeter drainage ditch south of the west entrance.
- Engineered fill excavated from the drainage ditch is hauled to the forebay footprint for construction of the pond berm.

Field Inspection Record

Job Number: 60265424 Date: July 3, 2012

Client: Newalta Corporation

Job Name: Stormwater Management System/ 7A Cell

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny / partial overcast, (28°C), slight breeze

progress:

**Detention /
Forebay Pond**

- Excavation of the perimeter drainage ditch along First Rd.
- Continued hauling engineered fill excavated from the drainage ditch to the forebay footprint for construction of the pond berm.

Field Inspection Record

Job Number: 60265424 **Date:** July 4, 2012

Client: Newalta Corporation

Job Name: East Landfill / Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 32°C

progress:

**Detention /
Forebay Pond**

- Continued excavation of the perimeter drainage ditch along First Rd.
- Construction of the forebay pond berm.
- Site meeting AECOM, Dufferin, Newalta (2:30-3:30).

Field Inspection Record

Job Number: 60265424 Date: July 5, 2012

Client: Newalta Corporation

Job Name: East Landfill / Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny, 35°C

progress:

**Detention/
Forebay Pond**

- Reviewed contractor GPS setup
- Excavating perimeter ditch south of First Rd entrance
- Hauling, placing & compacting eng. fill to form forebay
- Starting to clear brush from detention pond area

Field Inspection Record

Job Number: 60265424 **Date:** July 6, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 36°C

progress:

**Detention/
Forebay Pond**

- Excavating perimeter ditch south of First Rd entrance
- Hauling, placing & compacting eng. fill to form forebay
- Clearing brush from detention pond area

Field Inspection Record

Job Number: 60265424 **Date:** July 9, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 29°C

progress:

**Detention /
Forebay Pond**

- Excavating perimeter ditch south of First Rd entrance
- Hauling, placing & compacting eng. fill to form forebay

Field Inspection Record

Job Number: 60265424 Date: July 11, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny, 29°C

progress:

**Detention /
Forebay Pond**

- Hauling, placing & compacting eng. fill to form forebay & preparing for clay placement
- Placing & compacting clay liner of forebay
- Excavating perimeter ditch south of First Rd entrance

Field Inspection Record

Job Number: 60265424 Date: July 12, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny, 30°C

progress:**Detention /
Forebay Pond**

- Placing & compacting clay liner of forebay, 2nd lift completed

Field Inspection Record

Job Number: 60265424 **Date:** July 13, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Overcast, Sunny breaks, 31°C

progress:

**Detention/
Forebay Pond**

- Placing & compacting clay liner of forebay, completed by end of day

Field Inspection Record

Job Number: 60265424 **Date:** July 16, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 30°C

progress:

**Detention/
Forebay Pond**

- Excavating channel for forebay

Field Inspection Record

Job Number: 60265424 Date: July 18, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny, 28°C

progress:**Detention /
Forebay Pond**

- Stripping & stockpiling topsoil from detention pond area

Field Inspection Record

Job Number: 60265424 **Date:** August 1, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny to partly cloudy,(30°C),

progress:

<p><u>Detention/Forebay Pond</u> • Construction Site Meeting #3 in pm</p>
--

Field Inspection Record

Job Number: 60265424 Date: August 8, 2012

Client: Newalta Corporation

Job Name: Stormwater Management System/ 7A Cell

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Overcast,(28°C), slight breeze

progress:

- | | |
|--------------------------------------|---|
| <u>Detention/Forebay Pond</u> | <ul style="list-style-type: none">• Started excavating engineered fill from detention pond footprint.• Excavated engineered fill was hauled to the east buffer zone to be used for backfill. |
|--------------------------------------|---|

Field Inspection Record

Job Number: 60265424 **Date:** August 9, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Overcast, light rain in am, 25°C

progress:

**Detention /
Forebay Pond**

- Concrete culvert sections for perimeter drainage ditch delivered to site in AM.
- Continued excavating engineered fill from the detention pond footprint.

Field Inspection Record

Job Number: 60265424 **Date:** August 10, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Overcast, light rain in am, 22°C

progress:

- | | |
|--|--|
| <u>Detention /
Forebay Pond</u> | <ul style="list-style-type: none">• Clearing perimeter ditch @ First Rd entrance for culvert installation• Breaking rock @ detention pond |
|--|--|

Field Inspection Record

Job Number: 60265424 **Date:** August 13, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 27°C

progress:

**Detention/
Forebay Pond**

- Completed concrete culvert installation @ First Rd entrance
- Braking rock within the detention pond footprint and hauling to East buffer zone for backfill.

Field Inspection Record

Job Number: 60265424 **Date:** September 13, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 28°C

progress:

**Detention /
Forebay Pond**

- Hauling & placing/compacting clay PCL @ east end 7A
- 750 mm & 900 mm HDPE pipe delivered for Stormwater Management System.

Field Inspection Record

Job Number: 60265424 Date: September 19, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Sunny, 15°C

progress:**Detention /
Forebay Pond**

- Construction Site Meeting #4 in pm

Field Inspection Record

Job Number: 60265424 **Date:** September 25, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 20°C

progress:

**Detention/
Forebay Pond**

- Excavating detention pond area
- 8" perforated HDPE pipe delivered
- Constructing berm between ponds

Field Inspection Record

Job Number: 60265424 Date: September 28, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Overcast, 16°C

progress:

**Detention /
Forebay Pond**

- Placing & compacting eng. fill for detention pond

Field Inspection Record

Job Number: 60265424 **Date:** October 1, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 20°C

progress:

**Detention/
Forebay Pond**

- Placing & compacting eng. fill for detention pond & forebay

Field Inspection Record

Job Number: 60265424 Date: October 2, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Overcast, 18°C

progress:**Detention/
Forebay Pond**

- Placing & compacting eng. fill for detention pond & forebay

Field Inspection Record

Job Number: 60265424 **Date:** October 11, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 13°C

progress:

<u>Detention / Forebay Pond</u>	<ul style="list-style-type: none">• Excavating ditch south of forebay along First road• Started placing and compacting clay in detention pond
--	--

Field Inspection Record

Job Number: 60265424 **Date:** October 12, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 8°C

progress:

**Detention /
Forebay Pond**

- Excavating ditch south of forebay along First road
- Continued placing and compacting clay in detention pond

Field Inspection Record

Job Number: 60265424 **Date:** October 15, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: PC /High of 10°C

progress:

7A cell

- Continued placing and compacting clay in detention pond

Field Inspection Record

Job Number: 60265424 **Date:** October 16, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 12°C

progress:

**Detention/
Forebay Pond**

- Continued placing clay liner in detention pond

Field Inspection Record

Job Number: 60265424 Date: October 17, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker Personnel: See attached sheet

Weather: Overcast, rain, 10°C

progress:**Detention /
Forebay Pond**

- Placing & compacting clay in detention pond-completed by end of day

Field Inspection Record

Job Number: 60265424 **Date:** October 18, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: M. Coscarella/J. Munro/M. Stocker **Personnel:** See attached sheet

Weather: Sunny, 18°C

progress:

**Detention /
Forebay Pond**

- Clearing connection 6C/7A
- Grading Leachate collection blanket

Field Inspection Record

Job Number: 60265424 **Date:** October 22, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro / M. Coscarella **Personnel:** See attached sheet

Weather: Sunny, 18°C

progress:

**Detention /
Forebay Pond**

- Excavating perimeter ditch south of forebay
- Maintenance holes for the forebay and detention pond are delivered

Field Inspection Record

Job Number: 60265424 **Date:** October 24, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, rain, 12°C

progress:

**Detention/
Forebay Pond**

- Importing and stockpiling granular 'A' for LCS
- Other work limited due to weather
- Construction Site Meeting #5 in pm

Field Inspection Record

Job Number: 60265424 Date: October 26, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, cloudy ,17°C

progress:**Detention /
Forebay Pond**

- Placing & compacting clay in forebay channel

Field Inspection Record

Job Number: 60265424 **Date:** November 1, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, rain, 7°C

progress:

**Detention /
Forebay Pond**

- Removed old Catch Basin at First Road West and Green Mountain and replaced with new maintenance hole
- Connected outlet of new maintenance hole to existing culvert
- Started excavating trench and installing 750 mm HDPE pipe from catch basin, working east towards detention pond maintenance hole

Field Inspection Record

Job Number: 60265424 **Date:** November 2, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, showers, 7°C

progress:

**Detention /
Forebay Pond**

- Continue to excavate trench and install 750 mm HDPE pipe.
- Gabion baskets delivered to site.

Field Inspection Record

Job Number: 60265424 **Date:** November 5, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, 5°C

progress:

**Detention /
Forebay Pond**

- Continue to excavate trench and install 750 mm HDPE pipe.
- Installing detention pond Maintenance hole.
- Fine grading and proof rolling forebay.
- Orifice plate installed inside the maintenance hole within the detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 6, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, 6°C

progress:

**Detention/
Forebay Pond**

- Placing geotextile and rip rap at forebay channel.
- Fine grading and proof rolling remainder of forebay.
- Assembling gabion baskets.

Field Inspection Record

Job Number: 60265424 **Date:** November 7, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, cloudy periods, 14°C

progress:

**Detention/
Forebay Pond**

- Working on detention pond overflow weir.
- Placing and compacting clay base for over flow weir and in area for 300 mm PVC pipe.
- Assembling gabion baskets.

Field Inspection Record

Job Number: 60265424 **Date:** November 8, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, 7°C

progress:

**Detention /
Forebay Pond**

- Assembling and installing gabion baskets in forebay.
- Fine grading detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 9, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, 12°C

progress:

**Detention /
Forebay Pond**

- Completed gabion baskets within forebay.
- Completed rip rap placement in forebay.
- Assembling and installing gabion baskets in detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 12, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, rain in pm, windy 17°C

progress:

**Detention /
Forebay Pond**

- Assembling and installing gabion baskets in detention pond.
- Fine grading and compacting over flow weir.
- Installing geoweb at over flow weir.

Field Inspection Record

Job Number: 60265424 **Date:** November 13, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, cloudy periods, 4°C

progress:

**Detention/
Forebay Pond**

- Installing geoweb at overflow weir.
- Assembling and installing gabion baskets in detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 14, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, cloudy periods, 6°C

progress:

**Detention/
Forebay Pond**

- Installing and filling geoweb at overflow weir.
- Assembling and installing gabion baskets in detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 15, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro / M. Coscarella **Personnel:** See attached sheet

Weather: Overcast, 8°C

progress:

**Detention /
Forebay Pond**

- Installing and filling geoweb at overflow weir.
- Assembling and installing gabion baskets in detention pond.
- Placing and grading topsoil on outside banks of forebay.
- Installing 300 mm PVC pipe in detention pond Maintenance hole

Field Inspection Record

Job Number: 60265424 **Date:** November 16, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, 10°C

progress:

**Detention /
Forebay Pond**

- Installing and filling geoweb at overflow weir.
- Assembling and installing gabion baskets in detention pond.
- Placing and grading topsoil on outside banks of forebay and detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 19, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, foggy, 9°C

progress:

**Detention /
Forebay Pond**

- Placing and grading topsoil on outside banks of forebay and detention pond in am.
- Formed and poured concrete support pier for 300 mm PVC pipe at detention pond.

Field Inspection Record

Job Number: 60265424 Date: November 20, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Overcast, foggy, 10°C

progress:

**Detention/
Forebay Pond**

- Placing and compacting clay around 300 mm PVC pipe at detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 21, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, foggy, 9°C

progress:

**Detention/
Forebay Pond**

- Completed constructing support berm between forebay and detention pond.

Field Inspection Record

Job Number: 60265424 **Date:** November 22, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, 12°C

progress:

**Detention /
Forebay Pond**

- Placed armour stone around MH in detention pond

Field Inspection Record

Job Number: 60265424 **Date:** November 26, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, cloudy periods, 3°C

progress:

**Detention /
Forebay Pond**

- Excavating trench in support berm for 900 mm HDPE pipe between ponds
- Installing 900 mm pipe in late pm

Field Inspection Record

Job Number: 60265424 **Date:** November 30, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Overcast, windy, 5°C

progress:

**Detention/
Forebay Pond**

- 900 mm HDPE pipe complete from forebay to detention pond
- Compacting outside slopes of forebay and detention pond
- Continue perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: December 6, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, 2°C

progress:**Detention /
Forebay Pond**

- Surveyed forebay & detention pond area.

Field Inspection Record

Job Number: 60265424 Date: December 11, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Overcast, flurries, 0°C

progress:

**Detention/
Forebay Pond**

- Sluice gate delivered for maintenance hole within detention pond.

Field Inspection Record

Job Number: 60265424 Date: December 12, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, 3°C

progress:**Detention/
Forebay Pond**

- Installing orifice plate and sluice gate in detention pond Maintenance hole.

Field Inspection Record

Job Number: 60265424 **Date:** December 13, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, 4°C

progress:

**Detention /
Forebay Pond**

- Installing sluice gate in detention pond maintenance hole
- Continued with perimeter ditch excavation in pm.

Field Inspection Record

Job Number: 60265424 Date: December 14, 2012

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, windy, 6°C

progress:**Detention /
Forebay Pond**

- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 17, 2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, windy, 6°C

progress:**Detention /
Forebay Pond**

- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 18,2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, windy, 6°C

progress:**Detention /
Forebay Pond**

- Placing and grading topsoil on outside banks of forebay and detention pond in am.
- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 19,2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Partial Cloudy, windy, 12°C

progress:

**Detention /
Forebay Pond**

- Placing and grading topsoil on outside banks of forebay and detention pond in am.

Field Inspection Record

Job Number: 60265424 Date: April 22,2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, 7°C

progress:**Detention /
Forebay Pond**

- Placing and grading topsoil on outside banks of forebay and detention pond in am.
- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 23,2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, windy, 6°C

progress:**Detention /
Forebay Pond**

- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 24, 2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Sunny, 8°C

progress:**Detention /
Forebay Pond**

- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 25,2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Overcast, windy, 11°C

progress:**Detention /
Forebay Pond**

- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 26,2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Overcast, windy, 14°C

progress:**Detention /
Forebay Pond**

- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 Date: April 29, 2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro Personnel: See attached sheet

Weather: Overcast, 12°C

progress:**Detention /
Forebay Pond**

- Continued with perimeter ditch excavation

Field Inspection Record

Job Number: 60265424 **Date:** April 30,2013

Client: Newalta Corporation

Job Name: East Landfill Phase 7A

Contractor: Dufferin Construction

Inspected By: J. Munro **Personnel:** See attached sheet

Weather: Sunny, windy, 15°C

progress:

**Detention /
Forebay Pond**

- Completed stormwater management system.
- Approved for discharge of stormwater to road side ditch.